



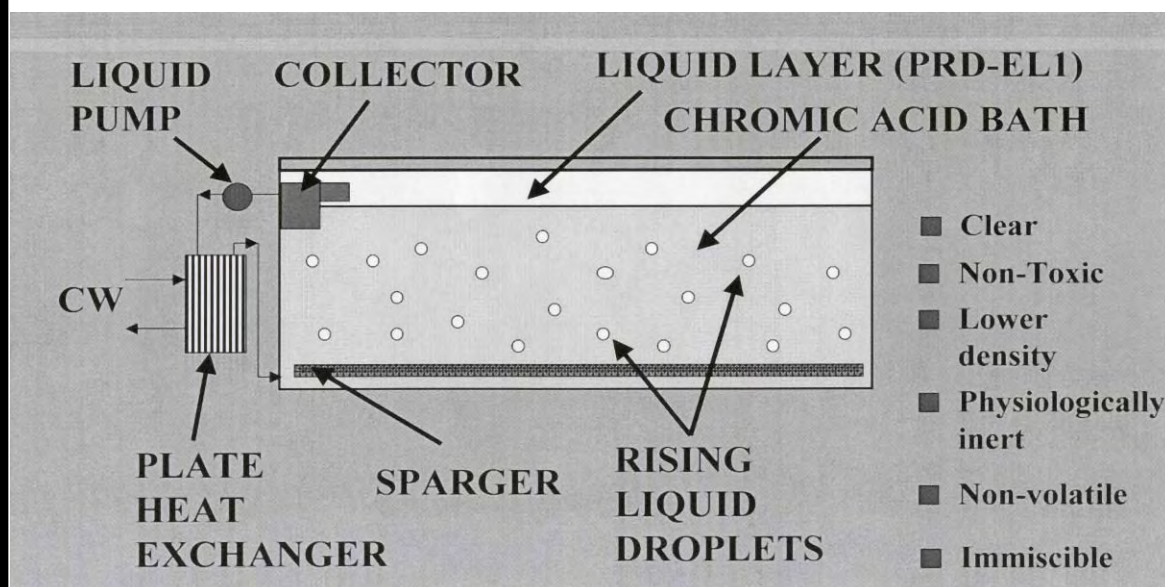
**US Army Corps  
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Engineer Research and  
Development Center

## Technology Demonstration of the Zero Emissions Chromium Electroplating System

### Appendix I: CHPPM Report on Air Sampling

K. James Hay, Stephen W. Maloney,  
John J. Cannon, Max R. Phelps, and  
Jason Modrell

February 2008



# **Technology Demonstration of the Zero Emissions Chromium Electroplating System, Appendix I: CHPPM Report on Air Sampling**

## **Final Report**

Approved for public release; distribution is unlimited.

Prepared for     U.S. Environmental Protection Agency  
                     26 West Martin Luther King Drive  
                     Cincinnati, OH 45268-0001

Under             Work Unit #CNE-B091

**ABSTRACT:** Volume 1 of this report documents the demonstration of a technology developed by PRD, Inc, for control of chromium emissions during hard chromium electroplating, the Zero Emissions System. The technology involves placing a blanket of a proprietary fluid, called PRD-EL1, on top of the plating bath. This fluid blanket prevents the formation of aerosols, which is the mechanism by which chromium is emitted from the plating bath to the air. The majority of the testing was directed at demonstration of the effectiveness of chromium plating in the presence of the immiscible blanket. Testing was conducted at Benét Laboratories on coupons and actual parts from Army vehicles. The results indicate that PRD-EL1 may cause deleterious effects on the plating process, as some of the parts failed qualitative tests performed at Benét. However, some parts, which were plated without the fluid blanket present as a baseline control, also failed the tests. Air sampling results indicate that the presence of the PRD-EL1 fluid reduced the chromium emissions to below the standard and the indoor air concentration below the previously established exposure limit but near the new exposure limit.. Overall, the results indicate that the use of the PRD process would require additional testing before it could be accepted for use in Army production and maintenance operations.

This second volume of the technical document is the Center for Health Promotion and Preventive Medicine's report on air sampling performed during the Zero Emission System's technology demonstration.

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# Preface

This study was conducted for Headquarters, Department of the Army, under Program Element 063728A, “Environmental Technology Demonstration”; Project 002, “Environmental Compliance Technology”; Work Unit CNE-B091, “Hazardous Air Pollutants Technology Demonstrations.” This project is part of the Army Environmental Quality Technology (EQT) Program. The ERDC technical reviewer was Hany Zaghloul, Program Manager.

The work was performed by the Environmental Processes (CN-E) Branch of the Installations Division (CN), Construction Engineering Research Laboratory (CERL). The CERL Principal Investigator was Dr. K. James Hay. Part of this work was done by Anniston Army Depot (POC: Tony Pollard), Benét Laboratories (POC: John Cannon), the Center for Health Promotion and Preventive Medicine (POC: Tim Hilyard), and PRD, Inc. (POC: Dr. Ramesh Melarkode). The technical editor was Linda L. Goersch, Information Technology Laboratory. Deborah Curtin is Chief, CN-E, and Dr. John T. Bandy is Chief, CN. Dr. Kirankumar V. Topudurti is Deputy Director of CERL and the Director of CERL is Dr. Ilker R. Adiguzel.

CERL is an element of the U.S. Army Engineer Research and Development Center (ERDC), U.S. Army Corps of Engineers. The Commander and Executive Director of ERDC is COL Richard B. Jenkins. The Director of ERDC is Dr. James R. Houston.

## Appendix I: CHPPM Report on Air Sampling



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MEMORANDUM FOR Commander, USACERL (W-ERDC-CERL-IL/Dr. Steve W. Maloney), U.S. Army Engineering Research and Development Center, Champaign, IL 61826-3482

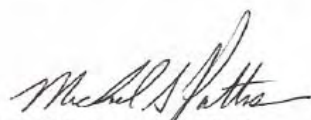
SUBJECT: Air Pollution Management Study No. 43-EL-5116-03, PRD Zero-Emission Process, Building 114, Anniston Army Depot, Alabama, 3-5 June 2003

Two copies of subject report with Executive Summary are enclosed.

The point of contact is Mr. Timothy Hilyard or the undersigned, DSN 584-2509/3500 or commercial (410) 436-2509/3500.

FOR THE COMMANDER:

Encl

*For*   
JAMES D. WOOD, P.E.  
Program Manager  
Air Quality Surveillance

CF:  
CDR, ANAD (AMSTA-AN-PECE/JEREMY TURNER)

# U.S. Army Center for Health Promotion and Preventive Medicine

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AIR POLLUTION MANAGEMENT STUDY  
NO. 43-EL-5116-03  
PRD ZERO-EMISSION PROCESS  
BUILDING 114  
ANNISTON ARMY DEPOT  
ANNISTON, ALABAMA  
3-5 JUNE 2003



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EXECUTIVE SUMMARY  
AIR POLLUTION MANAGEMENT STUDY  
NO. 43-EL-5116-03  
PRD ZERO-EMISSION PROCESS  
BUILDING 114  
ANNISTON ARMY DEPOT  
ANNISTON, ALABAMA  
3-5 JUNE 2003

1. PURPOSE. The purpose of this assessment is to determine the effectiveness of the Process Research and Development Technologies (PRD Tech. Inc) Zero-Emission Process in removing chromium (Cr) emissions from a full-scale chrome plating operation.
2. CONCLUSION. The average total Cr concentrations for each test series, as measured per the U.S. Environmental Protection Agency (USEPA) Method 306, was below the 0.015 milligram per dry standard cubic meter National Emission Standards for Hazardous Air Pollutants Cr standard.
3. RECOMMENDATIONS. Provide a copy of this report to the USEPA. If another demonstration is needed, conduct the testing without any other plating in progress during the demonstration. Also, a background test series should be conducted to determine how much Cr from the indoor air is exhausted out of the exhaust stack.

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# LIST OF ACRONYMS

ANAD	Anniston Army Depot
C	Celsius
CO <sub>2</sub>	carbon dioxide
Cr	chromium
DLS	Directorate of Laboratory Sciences
dscm	dry standard cubic meter
F	Fahrenheit
ft	foot
g	gram
GFAAS	Graphite Furnace Atomic Absorption Spectrometry
H <sub>2</sub> O	water
hr	hour
ICP-MS	inductively coupled plasma-mass spectroscopy
ID	inside diameter
in	inch
K	Kelvin
lb	pound
m <sup>3</sup>	cubic meter
mg	milligram
mL	milliliter
mm	millimeter
N <sub>2</sub>	nitrogen
NaOH	sodium hydroxide
NESHAP	National Emission Standards for Hazardous Air Pollutants
NIST	National Institute of Standards and Technology
O <sub>2</sub>	oxygen
PRD Tech. Inc.	Process Research and Development Technologies
QA/QC	quality assurance/quality control
RM	reference method
TSP	Total Suspended Particulate
USACHPPM	U.S. Army Center for Health Promotion and Preventive Medicine
USEPA	U.S. Environmental Protection Agency
°	degree
%	percent
μ	micro

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AIR POLLUTION MANAGEMENT STUDY  
NO. 43-EL-5116-03  
PRD ZERO-EMISSION PROCESS  
BUILDING 114  
ANNISTON ARMY DEPOT  
ANNISTON, ALABAMA  
3-5 JUNE 2003

1. REFERENCES. See Appendix A for a listing of references.
2. PURPOSE. The purpose of this assessment is to determine the effectiveness of the Process Research and Development Technologies (PRD Tech. Inc) liquid in removing chromium (Cr) emissions from a full-scale chrome plating operation.
3. GENERAL.
  - a. Background. Chrome plating of machinery parts produces a surface coating that helps reduce wear and corrosion. The military uses this process as a cheap and effective way to combat the wear and corrosion that parts suffer during usage. The problem with chrome plating is the emission of a fine aerosol, during the plating process. Once in the atmosphere, the aerosol forms chromic acid. Chrome has long been known to be a carcinogen and a cause of perforated nasal passages, skin rashes and other medical problems. The Cr emissions are currently controlled by capturing the aerosols at the surface using airflow directed across the plating vat. The air is pulled through an exhaust duct manifold (located on the opposite side of the vat) by an induced draft fan through an entrainment separator, and then exhausted from a stack outside the building. PRD Tech. Inc has developed a proprietary immiscible liquid that covers the top of the chrome bath during the plating process (see Figure 1). This liquid is designed to prevent the aerosols of Cr from reaching the atmosphere by trapping the bubbles before they reach the liquid-air interface. If successful, this process may replace expensive scrubber technology currently used to deal with Cr emissions.

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FIGURE 1. CHROME VAT WITH 4-INCHES OF PRD LIQUID



b. Facility Description. The Zero-Emission demonstration took place in Building 114 on the Anniston Army Depot (ANAD). This building houses the depot's metal finishing operations. Line 2 was used in this demonstration to allow for continued concurrent production on Line 1. Line 2 has a total of four chrome vats. For this demonstration only vats 12A and 12B were used.

c. Exhaust System Description. The exhausts from all the chrome vats join into one duct. The fumes are pulled through an induced draft fan and exhausted through an entrainment separator to a 38-inch inside diameter (ID) stack. For this demonstration, Alabama Department of Environmental Management (ADEM) has allowed the separator to be removed from this system.

d. U.S. Environmental Protection Agency (USEPA) Method 306 Sampling (Total Chrome).

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(1) Sampling Location. Line 2 of the Chrome Plating Finishing Complex exhausts to a 38-inch ID stack (see Figure 2). Two 4-inch ID ports, located at right angles to each other, are 114 inches (3 duct diameters) downstream and 53 ½ inches (1.4 duct diameters) upstream from the nearest flow disturbances (the induced draft fan and top of the stack, respectively). Per USEPA Reference Method (RM) 1 (reference 1), a velocity traverse of 24 sampling points (12 per traverse) was conducted using a pitot tube/thermocouple assembly. A cyclonic flow check was performed per USEPA RM 1 and was found to be acceptable. Velocity traverse and the cyclonic flow data are found in Appendix D.

FIGURE 2. LINE 2 EXHAUST STACK



(2) Sampling Procedures and Equipment. All sampling was conducted according to USEPA sampling methods. The USEPA RMs 1-4 (reference 1) were used to verify sampling points, conduct velocity traverse and cyclonic flow checks, and to determine moisture and stack gas content. Total chromium samples were collected according to USEPA Method 306 (reference 2). A detailed description of the sampling procedures and equipment used in the test is included in Appendix B.



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FIGURE 3. TSP-WEST LOCATION



FIGURE 4. TSP-EAST LOCATION



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(3) Sample Recovery and Analysis. The procedures for recovery and analysis of all samples are discussed in Appendix C. The U.S. Army Center for Health Promotion and Preventative Medicine (USACHPPM) contract lab, Severn Trent Laboratory located in Sacramento, California, performed USEPA RM 306 analyses.

e. Indoor Ambient Air Sampling. At the request of the USEPA, Total Suspended Particulate (TSP) samplers were used to determine the Cr levels in the indoor atmosphere.

(1) Sampling Location. Two high-volume TSP samplers were sited on the chrome plating line in Building 114. The West sampler was located approximately six feet west of chrome plating vat 12B (SN K0966). The East sampler was located approximately 12 feet east of chrome plating vat 12B. Both locations are shown in Figures 3-5.

(2) Sampling Procedures and Equipment. High-Volume TSP samplers were used to collect air samples from the atmosphere inside of Building 114. The sampling was to determine the emissions generated from the chromic acid used in the chrome plating operation. The TSP is considered to be all airborne solid and low vapor pressure liquid particles (mist) with an aerodynamic particle size ranging from approximately  $0.8\mu\text{m}$  to greater than  $100\mu\text{m}$ . All TSP samples were collected according to Title 40, Code of Federal Regulations (CFR) 50, Appendix B, Reference Method for the Determination of Suspended Particulate Matter in the Atmosphere (High-Volume Method) (reference 6). The sampling team used two Graseby-Andersen Model GT2200 high-volume TSP samplers to sample for Cr. The TSP sampler operated by drawing a measured quantity of ambient air into a covered housing and through an 8 x 10-inch quartz fiber filter for a two hour sample duration. Two-hour samples were collected to coincide with the stack sampling run times. A total of nine samples were collected with each sampler.

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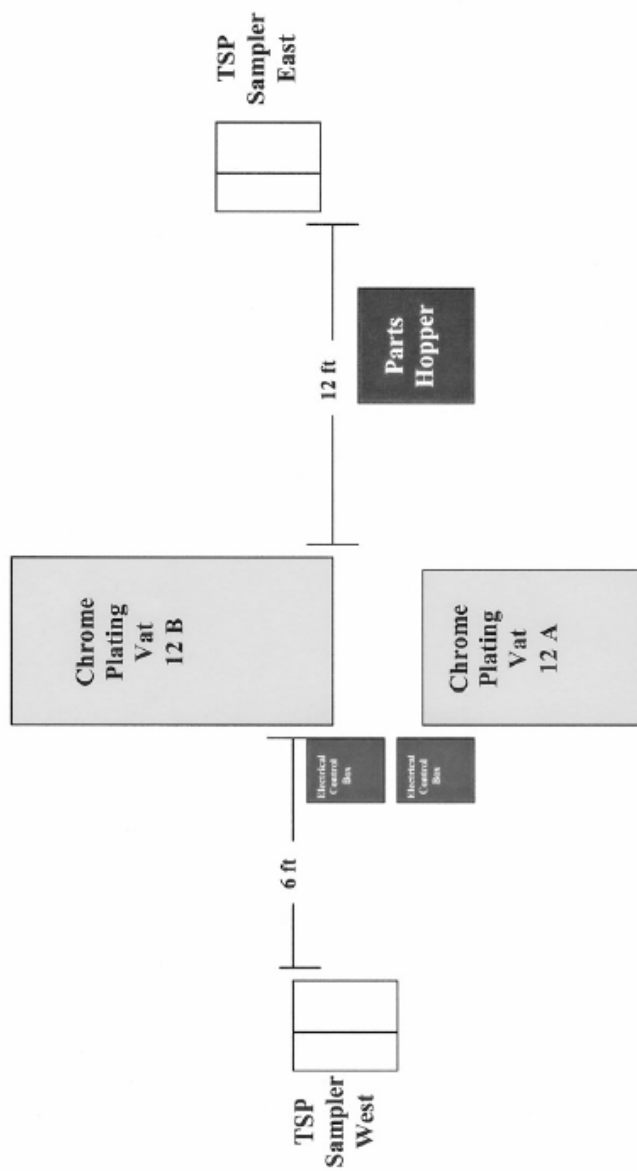


FIGURE 5. CHROME PLATING LINE 2 - TSP SPECIFIC SAMPLER LOCATIONS



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(3) Sample Recovery and Analysis. The procedures for recovery and analysis of all samples are discussed in Appendix C. At the conclusion of the ambient air-sampling mission, all filters were hand-carried by the ambient air sampling team back to USACHPPM. The USACHPPM Directorate of Laboratory Sciences (DLS) Analytical Spectrometry Division (ASD) analyzed the filters for Cr.

f. Test Series. The three test series conducted are described in Table 1.

TABLE 1. TEST SERIES

TEST SERIES	DESCRIPTION
Test Series 1	4-inches of PRD Liquid
Test Series 2	2-inches of PRD Liquid
Test Series 3	No PRD Liquid

g. Assessment Personnel. The USACHPPM personnel participating in the field assessment are shown in Table 2.

TABLE 2. USACHPPM ASSESSMENT PERSONNEL

PERSONNEL	MAJOR DUTIES/RESPONSIBILITIES
Tim Hilyard	Project Officer
Joe Simonovitch	Engineering Technician
Joe Sutphin	Engineering Technician
Mike McCarter	Physical Science Technician

h. Nomenclature and Equations. The nomenclature and equations used for this assessment are found in Appendix E.

#### 4. FINDINGS AND DISCUSSION.

##### a. Non-Standard Events.

(1) Run 1. During Run 1, chrome plating was occurring in a vat on line 2 which was not being used for this demonstration. Because of this condition, the results for this run may be biased high. The vat was on line 2 and was covered with plastic for the duration of the study.

(2) Run 4 was started at 0820, however vat 12B was not turned on until 0900. Thus, the plating was not maximized for this entire run. This could lead to the emissions being biased low.

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(3) Run 7, 8, and 9.

(a) For the test series with no PRD-liquid (Runs 7, 8, and 9), there was still some left over PRD-liquid in the tanks. This could lead to a potential low bias in the emissions.

(b) During Runs 7, 8, and 9 the large vat at the end of Line 1 was plating. Potential fumes from this operation, if introduced into the Line 2 exhaust stack, could bias the results high.

b. Data Summary. Field data sheets for all sampling runs are found in Appendix F and G.

c. Plating Items. For this demonstration test coupons were plated for 12 hours.

d. Emission Data. The average total Cr emission data, as tested, is summarized in Table 3. This data may have been biased by events discussed in section a. Cr emission data can be found in Appendix K.

TABLE 3. AVERAGE TOTAL CHROME CONCENTRATIONS

Test Series	4-Inches of PRD Liquid (Runs 1-3)	2-Inches of PRD Liquid (Runs 4-6)	No PRD Liquid (Runs 7-9)
<u>Amperage</u>			
Vat 12A	1,100	1,100	1,100
Vat 12B	267	300	300
Total Amperage	1,367	1,400	1,400
<u>STACK EMISSION DATA</u>			
Actual Total Cr Concentration (mg/dscm)	0.011	0.008	0.014
NESHAP Cr Standard (mg/dscm)	0.015	0.015	0.015
<u>TSP SAMPLER DATA</u>			
Total Cr			
TSP-West (mg/m <sup>3</sup> )	0.046	0.016	0.100
TSP-East (mg/m <sup>3</sup> )	0.025	0.005	0.019

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(1) Test Series 1. The first test series consisted of three runs with 4-inches of PRD liquid in the chromium vats. The average emission data for the 4-inches of PRD liquid Test Series can be found in Table 3. Individual run data is found in Table 4.

(a) USEPA Method 306. The average concentration of total Cr for the three runs was 0.011 mg/dscm. The concentration for each individual run was 0.016 mg/dscm, 0.009 mg/dscm and 0.007 mg/dscm, respectively.

(b) TSP Samplers. The average concentrations of total Cr for the three runs were 0.046 mg/m<sup>3</sup> and 0.025 mg/m<sup>3</sup> for the TSP-West and TSP-East respectively. The TSP-West had concentrations of 0.125 mg/m<sup>3</sup>, 0.010 mg/m<sup>3</sup>, and 0.004 mg/m<sup>3</sup> for the individual run. The TSP-East had concentrations of 0.067 mg/m<sup>3</sup>, 0.005 mg/m<sup>3</sup>, and 0.002 mg/m<sup>3</sup> for each run.

TABLE 4. TOTAL CHROME CONCENTRATIONS 4-INCHES OF PRD LIQUID

Run Number	Run 1	Run 2	Run 3
<u>Amperage</u>			
Vat 12A	1,100	1,100	1,100
Vat 12B	200	300	300
Total Amperage	1,300	1,400	1,400
<u>STACK EMISSION DATA</u>			
Total Cr			
Concentration (mg/dscm)	0.016	0.009	0.007
<u>TSP SAMPLER DATA</u>			
Total Cr			
TSP-West (mg/m <sup>3</sup> )	0.125	0.010	0.004
TSP-East (mg/m <sup>3</sup> )	0.067	0.005	0.002

(2) Test Series 2. A two-inch thickness of PRD liquid was used for Series 2. Average emission data for the 2-inches of PRD liquid test series can be found in Table 3 and individual run data in Table 5.

(a) USEPA Method 306. The average Cr concentration for the three runs was 0.008 mg/dscm. The concentrations were

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0.011 mg/dscm, 0.004 mg/dscm, and 0.008 mg/dscm for Runs 4-6 respectively.

(b) TSP Samplers. The average total Cr concentration for the three runs was 0.016 mg/m<sup>3</sup> and 0.005 mg/m<sup>3</sup> for TSP-West and TSP-East, respectively. TSP-West had concentrations of 0.020 mg/m<sup>3</sup>, 0.019 mg/m<sup>3</sup>, and 0.009 mg/m<sup>3</sup> for each run. While TSP-East had concentrations of 0.006 mg/m<sup>3</sup>, 0.005 mg/m<sup>3</sup>, and 0.004 mg/m<sup>3</sup> for each run.

TABLE 5. TOTAL CHROME CONCENTRATIONS 2-INCHES OF PRD Liquid

Run Number	Run 4	Run 5	Run 6
<u>Amperage</u>			
Vat 12A	1,100	1,100	1,100
Vat 12B	300	300	300
Total Amperage	1,400	1,400	1,400
<u>STACK EMISSION DATA</u>			
Total Cr			
Concentration (mg/dscm)	0.011	0.004	0.008
<u>TSP SAMPLER DATA</u>			
Total Cr			
TSP-West (mg/m <sup>3</sup> )	0.020	0.019	0.009
TSP-East (mg/m <sup>3</sup> )	0.006	0.005	0.004

(3) Test Series 3. The third test series consisted of three runs with no PRD liquid in the chromium vats. Average Emission data is found in Table 3 and individual run data is found in Table 6.

(a) USEPA RM 306. 0.014 mg/dscm was the average Cr concentration for the three runs. Runs 7-9 concentrations were 0.013 mg/dscm, 0.013 mg/dscm, and 0.015 mg/dscm, respectively.

(b) TSP Samplers. The average total Cr concentration for the three runs was 0.100 mg/m<sup>3</sup> and 0.019 mg/m<sup>3</sup> for the TSP sampler West and TSP sampler East respectively. TSP sampler West had total chrome concentrations of 0.130 mg/m<sup>3</sup>, 0.098 mg/m<sup>3</sup>, and



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0.071 mg/m<sup>3</sup>. TSP sampler East had concentrations of 0.027 mg/m<sup>3</sup>, 0.021 mg/m<sup>3</sup>, and 0.011 mg/m<sup>3</sup> for each run.

e. Sampling/Analytical Techniques. A summary of the sampling and analysis performed for this PRD Zero-Emission Study is found in Table 7.

TABLE 6. TOTAL CHROME CONCENTRATIONS NO PRD LIQUID

Run Number	Run 7	Run 8	Run 9
<u>Amperage</u>			
Vat 12A	1,100	1,100	1,100
Vat 12B	300	300	300
Total Amperage	1,400	1,400	1,400
<u>STACK EMISSION DATA</u>			
Total Cr Concentration (mg/dscm)	0.013	0.013	0.015
<u>TSP SAMPLER DATA</u>			
Total Cr TSP-West (mg/m <sup>3</sup> )	0.130	0.098	0.071
TSP-East (mg/m <sup>3</sup> )	0.027	0.021	0.011

TABLE 7. SAMPLING/ANALYTICAL TECHNIQUES

POLLUTANT CATEGORY	SAMPLING METHOD	ANALYSIS METHOD	CONSTITUENTS TO BE DETERMINED
Total Cr	USEPA Method 306	GFAAS	Total Cr
Total Cr	TSP Samplers	ICP-MS	Total Cr

(1) Sampling Procedures. The sampling procedures used during the PRD Zero-Emission Study are detailed in Appendix B.

(2) Sampling Duration/Volumes. The sampling durations and sample volumes for each of the trains can be found in Appendix F.

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f. Sampling/Analytical Quality Assurance (QA)/Quality Control (QC).

(1) QA/QC objectives. The QA/QC objectives and methods for this Treatability Study are provided in the following paragraphs.

(2) USEPA RM 306 Procedures. The QA/QC for emission sampling consisted primarily of performing necessary calibrations per references 1 and 7 and operating stack-sampling equipment per reference 1. Appendix I contains a summary of the calibration data. The QA/QC procedures for this train included analysis of media blanks such as the filter and reagents. The blank analytical results are provided in Appendix H.

(3) TSP Samplers.

(a) Equipment Calibration. The high-volume TSP samplers were calibrated and checked for leaks at the staging area prior to set up at the sample sites. A calibrated orifice transfer standard kit, traceable to NIST, was used to calculate each sampler's flow parameters. Calibration of the two high-volume samplers yielded acceptable correlation coefficients ( $r$ ) greater than 0.990, as required by 40 CFR Part 50, Appendix B (reference 6). Flow checks were performed at the beginning and end of each sampling event to ensure proper equipment operation. Periodic flow checks during sampling events were also performed. Valid samples had flow rates between 1.1 and 1.7 m<sup>3</sup>/minute, and a total sample time of 2 hrs. The results of the flow checks were entered on TSP field data sheets (see Appendix G).

(b) Sample Preservation. Prior to field use, all quartz fiber filters were visually inspected for tears and pinholes. Each filter was then placed in individual, protective filter envelopes. While at ANAD all filters were maintained in their envelopes and stored in the chemistry laboratory in Building 114. All filters were prepared and recovered in this same room.

(c) Sample Validation Criteria. All sample run times were within the two-hour sample duration as well as the required flow rate of 1.1 - 1.7 cubic meters per minute (m<sup>3</sup>/min). All calibration criteria were met, to include that no single point flow check was greater than +/- 10% deviation and sampler regression coefficients were greater than 0.99.

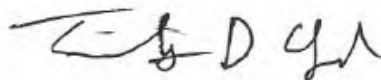
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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

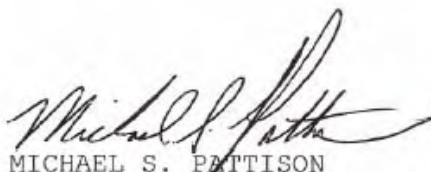
g. Sample Custody. The integrity of the samples was maintained with completed sample chain-of-custody sheets. These sheets provided a unique sample number, volumes, and descriptions for each sample. The custody sheets also specified names of sample custodians, dates, and run numbers. Appendix J includes the sample custody sheets.

5. CONCLUSION. The average total Cr concentrations for each test series, as measured per USEAP Method 306, was below the 0.015 milligram per dry standard cubic meter (mg/dscm) National Emission Standards for Hazardous Air Pollutants (NESHAP) Cr standard.

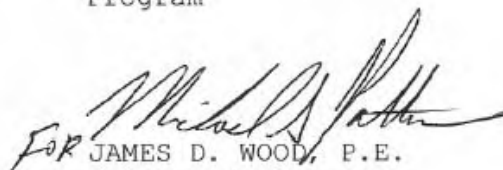
6. RECOMMENDATIONS. Provide a copy of this report to the USEPA. If another demonstration is needed, conduct the testing without any other plating in progress during the demonstration. Also a background test series should be conducted to determine how much chromium from the indoor air is exhausted out of the exhaust stack.



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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

#### APPENDIX A

#### REFERENCES

1. Title 40 CFR, 1998 Revision, Part 60 Appendix A, Reference Methods.
  2. Title 40 CFR, 2001 Revision, Part 63 Appendix A, Test Methods.
  3. Test Methods for Evaluating Solid Waste, SW-846, Third Edition, December 1996, USEPA.
  4. USEPA, Manual APTD-0576, March 1983, Maintenance, Calibration, and Operation of Isokinetic Source Sampling Equipment.
  5. USEPA, Publication No. 600/4-77-027B, March 1983, Quality Assurance Handbook for Air Pollution Measurement Systems, Volume II, Stationary Source Specific Methods.
  6. Title 40 CFR, 1998 Revision, Part 50, Appendix B, Reference Method for the Determination of Suspended Particulate Matter in the Atmosphere (High Volume Method).
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APPENDIX B

SAMPLING EQUIPMENT AND PROCEDURES

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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

1. STACK SAMPLING EQUIPMENT. The USEPA RM 306 (reference 2) will be used to measure the Cr emissions being released to the atmosphere at the stack. The train configuration is as follows:

- Pyrex® sample nozzle
- Teflon® union
- Pyrex lined probe sheath assembly
- Teflon® flex line
- 90° elbow
- Impinger No. 1-100 mL 0.1 N NaOH solution
- 180° glass connector
- Impinger No. 2-100 mL 0.1 N NaOH solution
- 180° glass connector
- Impinger No. 3-dry
- 180° glass connector
- Impinger No. 4-silica gel

S-type pitot tubes and thermocouples will be attached to the sampling probe. The pitot tubes will be 0.75-in. from the probe nozzle, and the thermocouples will be placed to eliminate any disturbance in the velocity measurements. The probe will be attached to a sample box containing the impinger train by a Teflon flex line. The impingers will be packed in an ice bath to cool the gas and to remove the moisture from the gas sample. The sample box will be connected to an umbilical cord, which contains the vacuum line, pitot lines, electrical connections and thermocouple wires. The meter box has a calibrated dry gas meter and calibrated orifice. A vacuum pump will be used to draw the sample through the sampling equipment. Two manometers, mounted on the meter box, will measure the velocity pressure in the stack and the pressure differential across the meter box orifice.

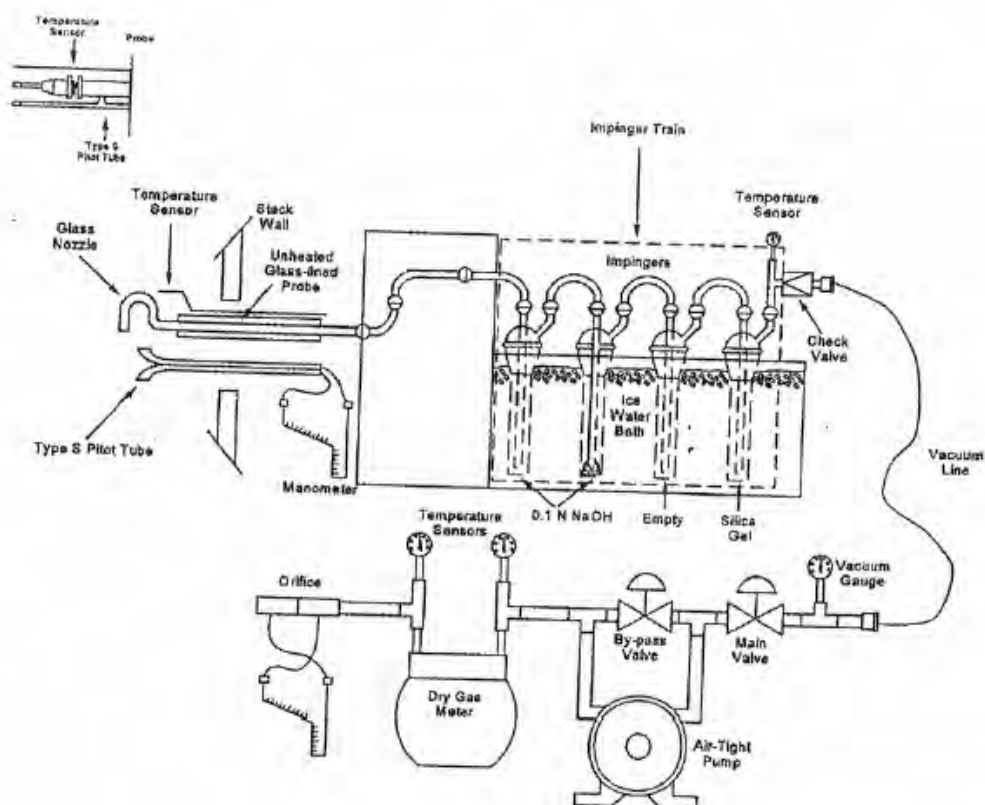
2. STACK SAMPLING PROCEDURES. Traverse points were determined and a preliminary velocity, temperature, and cyclonic flow traverse was conducted in accordance with USEPA RMs 1 and 2 of reference 1. Following these initial traverses, nine separate sampling runs were performed according to USEPA RM 306. The USEPA RM 306 sampling train will be operated isokinetically. Sampling will be performed by controlling the sampling flow rates, so the velocities of the gases entering the sampling nozzle are equal (within  $\pm 10\%$ ) to those of the undisturbed stack gas stream at the sampling points. Since this is not a fuel burning source, gas composition will be considered as ambient air (i.e., 79 percent  $N_2$ , and 21 percent  $O_2$ ).

® Pyrex is registered trademark of Corning Glass Works, Houghton Park, Corning, New York

® Teflon is a registered trademark of E.I. DuPont de Nemours & Co., Inc., Wilmington, Delaware.

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#### Impinger Contents

Impinger 1 - 100 mL 0.1 N NaOH  
Impinger 2 - 100 mL 0.1 N NaOH  
Impinger 3 - Initially Dry  
Impinger 4 - Silica Gel

FIGURE 1. USEPA RM 306 Sampling Train

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3. SAMPLING POINTS. The Line 2 stack is 38 inches ID. Two 4-inch ID sampling ports were installed on the exhaust stack approximately 53 ½ inches (1.4 duct diameters) from the nearest upstream disturbance (the top of the stack) and 114 inches (3 duct diameters) from the nearest downstream disturbance (the exhaust fan). Based on the disturbances and USEPA RM 1, a total of 24 traverse points were to be sampled. Stack velocity pressure and temperature readings were taken every 5 minutes throughout each 2-hour run. Figure B-3 shows the preliminary velocity/temperature traverse point locations within the stack and the approximate sampling location during the single point sampling runs.

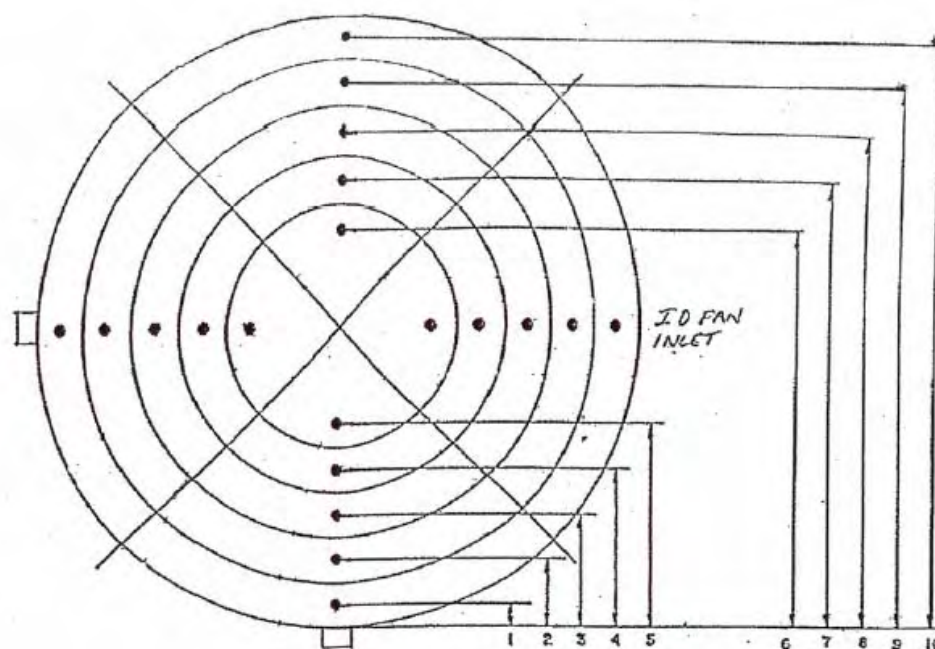
4. STACK GAS MOISTURE. Moisture was collected in the impingers of each sample train. All impingers were kept in an ice bath so that the final impinger stack gas exit temperature did not exceed 68 °F. Total moisture was determined by weighing the impingers and contents before and after each run. The weight, in grams, gained by the impingers was equal to the volume, in mL, collected during the run. The impingers were weighed on a top loading balance accurate to 0.1 gram.

5. STACK GAS COMPOSITION. Since this is not a fuel burning source, gas composition will be considered as ambient air (i.e., 79 percent N<sub>2</sub>, and 21 percent O<sub>2</sub>).

6. TSP SAMPLERS. High-Volume Total Suspended Particulate (TSP) samplers (see Figure 1) were used to collect air samples from the atmosphere inside of Building 114. The sampling was to evaluate the emissions generated from the chromic acid used in the chrome plating operation. TSP is considered to be all airborne solid and low vapor pressure liquid particles (mist) with an aerodynamic particle size ranging from approximately 0.8µm to greater than 100µm. All TSP samples were collected according to Title 40, Code of Federal Regulations (CFR) 50, Appendix B, Reference Method for the Determination of Suspended Particulate Matter in the Atmosphere (High-Volume Method) (reference 5). The sampling team used two Graseby-Andersen Model GT2200 high-volume TSP samplers to sample for Chromium. The TSP sampler operated by drawing a measured quantity of ambient air into a covered housing and through an 8 x 10 inch quartz fiber filter for a two hour sample duration. Two-hour samples were collected to coincide with the stack sampling run times. A total of nine samples were collected with each sampler.

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<u>Point No.</u>	<u>Percentage of Stack Diameter</u>	<u>Distance From Stack Wall</u>
1,13	2.1	7/8"
2,14	6.7	2 1/2"
3,15	11.8	4 1/2"
4,16	17.7	6 3/4"
5,17	25.0	9 1/2"
6,18	35.6	13 1/2"
7,19	64.4	24 1/2"
8,20	75.0	28 1/2"
9,21	82.3	31 1/4"
10,22	88.2	33 1/2"
11,23	93.3	35 1/2"
12,24	97.9	37 1/8"

Figure B-3. Preliminary Traverse Point and Sampling Locations for ANAD Line 2 Exhaust Stack

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APPENDIX C  
SAMPLE RECOVERY AND ANALYSIS

1. STACK GAS.

a. Stack Gas Composition. Since this is not a fuel burning source, gas composition will be considered as ambient air (i.e., 79 percent N<sub>2</sub>, and 21 percent O<sub>2</sub>).

b. Stack Gas Moisture Determination. Moisture was collected in the impingers of each sample train. All impingers were kept in an ice bath so that the final impinger stack gas exit temperature did not exceed 68 °F. Total moisture was determined by weighing the impingers and contents before and after each run. The weight, in grams, gained by the impingers was equal to the volume, in mL, collected during the run. The impingers were weighed on a top loading balance accurate to 0.1 gram.

2. USEPA RM 306 DETERMINATION. Total chromium emissions were collected using RM 306 (reference 2) sampling trains.

a. Sample 1. Measured the volume of the first, second, and third impingers, then quantitatively transferred the liquid into a labeled sample container (Container 1). Rinsed the probe nozzle, probe liner, flex line, the three impingers and connecting glassware with approximately 200 to 300 mL of 0.1 N NaOH. This rinse was added to Container 1. Then, placed a signed and dated sample custody seal over the lid and top of jar to ensure the lid is not removed prior to the analytical lab receiving the sample.

3. TSP SAMPLER. The indoor chromium was collected using TSP samplers. The sampler operates by drawing a measured quantity of ambient air into a covered housing and through an 8 x 10 inch QMA quartz fiber filter for a desired sample period. Chromium samples were prepared according to 40 CFR 50, Appendix G (reference 6). Any Chromium collected was leached off the filter with a diluted nitric acid solution on a hot plate for approximately 30 minutes and then analyzed by USEPA Method 200.8-Inductively Coupled Plasma-Mass Spectrometry (IPC-MS). The concentration of Chromium was determined by dividing the reported mass by the volume of air drawn through the filter during the sampling period. A field blank and a trip blank were submitted with the batch of samples.

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#### APPENDIX D

TRAVERSE POINT, VELOCITY TRAVERSE AND CYCLONIC FLOW DATA

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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## STACK GAS VELOCITY AND CYCLONIC FLOW DATA

INSTALLATION/PROJECT NUMBER: Anniston Army Depot, Alabama / 43-EL-5116-03			DATE: 3 June 2003	
SAMPLING LOCATION: Chrome Plating Finishing Complex BLDG 114			TIME: 0845	
OPERATOR: H. I. yard	AMBIENT TEMP (°F) 70°F	P <sub>bar</sub> (in. Hg)	P <sub>stat</sub> (in. H <sub>2</sub> O)	
MOLECULAR WT (lb/lb mole)	EXHAUST STACK ID (in.)		PITOT TUBE C <sub>p</sub> 0.84	
	ID SIDE 1 38"	ID SIDE 2 38"		

TRAVERSE POINT		POSITION (in.)	STACK GAS VELOCITY HEAD (in. H <sub>2</sub> O)		STACK GAS TEMPERATURE (°F)		YAW ANGLE (°)	
1	13		0.310	0.430	76	77	13° 8'	12°
2	14		0.310	0.430	76	77	16° 12'	18°
3	15		0.350	0.428	76	78	13°	2°
4	16		0.360	0.360	76	76	15°	22°
5	17		0.350	0.31	77	76	16°	19°
6	18		0.300	0.30	78	76	10°	5°
7	19		0.320	0.32	77	76	22°	11°
8	20		0.360	0.34	77	76	13°	15°
9	21		0.340	0.34	77	76	11°	23°
10	22		0.400	0.36	77	77	18°	18°
11	23		0.430	0.37	77	76	17°	18°
12	24		0.430	0.37	77	77	15°	18°
AVERAGES			0.359 "H <sub>2</sub> O		77 °F		14°	



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## TRAVERSE POINT LOCATION FOR CIRCULAR STACKS

INSTALLATION: Anniston Army Depot, Alabama

PROJECT NUMBER: 43-EL-5116-03

DATE: 2 June 03 SAMPLING LOCATION: Chrome Plating Finishing Complex, BLDG 114

INSIDE OF FAR WALL TO OUTSIDE  
OF NIPPLE (DISTANCE A): 38"INSIDE OF NEAR WALL TO OUTSIDE  
OUTSIDE OF NIPPLE (DISTANCE B): 0"

STACK I.D. (A - B): 38"

NEAREST UPSTREAM DISTURBANCE: 114"

NEAREST DOWNSTREAM DISTURBANCE: 53 1/2" (1.4 dd) 64" (3 dd) 114" (3 dd)

PITOT TUBE BLOCKAGE CORRECTION FACTOR:

External Sheath and % Blockage > 3%  $K = 1.0197 - 0.0098 (\% \text{ Blockage})$ No External Sheath and % Blockage > 2%  $K = 1.0132 - 0.0101 (\% \text{ Blockage})$ 

% Blockage = (Stack Dia/2 - Nozzle Length) (Sheath Dia) / Stack Area X 100

$$C_{p_{cor}} = 0.84 K$$



SCHEMATIC OF SAMPLING LOCATION

Traverse Point Number	Fraction of Stack ID	Stack ID	Traverse Point Location (To Nearest 1/8")	Distance B	Traverse Point Location From Outside Nipple
1/13	2.1	38"	7/8	0"	7/8
2/14	6.7		2 1/2		2 1/2
3/15	11.8		4 1/2		4 1/2
4/16	17.7		6 3/4		6 3/4
5/17	25.0		9 1/2		9 1/2
6/18	35.6		13 1/2		13 1/2
7/19	64.4		24 1/2		24 1/2
8/20	75.0		28 1/2		28 1/2
9/21	82.5		31 1/4		31 1/4
10/22	88.2		33 1/2		33 1/2
11/23	93.7		35 1/2		35 1/2
12/24	97.9		37 1/8		37 1/8

APPENDIX E  
NOMENCLATURE AND EQUATIONS

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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## NOMENCLATURE

SYMBOL	UNITS	DESCRIPTION
$A_n$	ft <sup>2</sup>	Cross-sectional area of nozzle
$A_s$	ft <sup>2</sup>	Cross-sectional area of stack
$B_{w0}$	decimal	Mole fraction of stack as water content
$C_m$	mg/dscm	chromium concentration of stack gas
$C_p$	-	S-type pitot tube coefficient
$C_{TSP}$	mg/m <sup>3</sup>	chromium concentration of TSP Sampler
$CO_2$	%	Concentration of CO <sub>2</sub> in gas stream as measured by an orsat analyzer, dry basis
$\Delta H$	inches H <sub>2</sub> O	Average pressure drop across the meter box orifice
$I$	%	The ratio of the sampling velocity to the stack velocity, 100% when the two are equal
$M_m$	mg	Mass of chromium collected
$M_s$	lb/lb mole	Molecular weight of stack gas
$N_2$	%	Concentration of N <sub>2</sub> in gas stream as determined by an orsat analyzer, dry basis
$O_2$	%	Concentration of O <sub>2</sub> in gas stream as measured by an orsat analyzer, dry basis
$\Delta P$	inches H <sub>2</sub> O	Velocity head of stack gas
$P_{bar}$	inches Hg	Barometric pressure at local elevation
$P_m$	inches Hg	Absolute pressure ( $P_{bar} + \Delta H/13.6$ ) at meter
$P_s$	Inches Hg	Absolute pressure ( $P_{bar} + P_{stat}/13.6$ ) at stack

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SYMBOL	UNITS	DESCRIPTION
$P_{stat}$	Inches H <sub>2</sub> O	Static pressure in stack
$Q_s$	dscf/hr	Average stack gas volumetric flow rate, dry, at standard conditions
$T_m$	°R	Average dry gas meter temperature (°F + 460)
$T_s$	°R	Average stack gas temperature (°F + 460)
$T_{std}$	°R	Standard absolute temperature, 528°F
$V_{lc}$	g	Total mass of liquid collected in the impingers and silica gel
$V_m$	ft <sup>3</sup>	Volume of gas through the dry gas meter at meter conditions
$V_{m\ std}$	dscf	Volume of dry gas sampled at standard conditions
$V_s$	ft/sec	Average stack gas velocity at sampling site
$V_{std}$	M <sup>3</sup>	Volume pulled through the TSP samplers
$V_{w\ std}$	scf	Water vapor volume at standard conditions
$W_n$	mg/m <sup>3</sup>	Net weight of TSP filters
$\theta$	min	Total sampling time per run
$\gamma_m$	-	Dry gas meter coefficient

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# EQUATIONS

1. ABSOLUTE PRESSURE,  $P_m$  and  $P_s$  (inches Hg).

$$P_m = P_{bar} + \frac{\Delta H}{13.6}$$

$$P_s = P_{bar} + \frac{P_{static}}{13.6}$$

2. DRY GAS METER VOLUME, STANDARD CONDITIONS,  $V_{mstd}$  (dscf).

$$V_{mstd} = \frac{17.65 V_m \gamma_m P_m}{T_m}$$

3. WATER VAPOR VOLUME, STANDARD CONDITIONS,  $V_{wstd}$  (scf).

$$V_{wstd} = 0.04707 V_{lc}$$

4. MOISTURE CONTENT,  $B_{wo}$  (percent).

$$B_{wo} = \frac{V_{wstd}}{V_{mstd} + V_{wstd}}$$

5. STACK GAS MOLECULAR WEIGHT,  $M_s$  (lb/lb-mole).

$$M_s = (1 - B_{wo}) [0.44(\%CO) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO_2)] + 18 B_{wo}$$


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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June

6. AVERAGE STACK GAS VELOCITY,  $v_s$  (ft/sec).

$$v_s = 85.48 C_p (\Delta P^{0.5})_{avg} \left( \frac{T_s}{P_s M_s} \right)^{0.5}$$

7. AVERAGE STACK GAS VOLUMETRIC FLOW RATE,  $Q_s$  (dscf/hr).

$$Q_s = \frac{63,529 (1 - B_{wo}) (V_s) (A_s) (P_s)}{T_s}$$

8. ISOKINETIC SAMPLING RATE,  $I$  (percent).

$$I = \frac{0.0945 (T_s) (V_{std})}{\theta V_s P_s A_s (1 - B_{wo})}$$

9. STACK CHROMIUM CONCENTRATION,  $C_m$  (mg/dscm)

$$C_m = \frac{35.51 M_m}{V_{std}}$$


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10. TSP SAMPLER CHROMIUM CONCENTRATION, (mg/m<sup>3</sup>)

$$C_{TSP} = \frac{W_N}{V_{STD}}$$

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APPENDIX F

SAMPLING TRAIN DATA SUMMARY

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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

SAMPLING DATA AND ISOKINETIC SHEETS

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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

# ISOKINETIC DATA SHEET<sup>1</sup>

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 3 Jun

LOCATION: Chrome Plating Finishing Complex, BLDG 114 RUN NUMBER: 1

## FROM FIELD DATA SHEET:

$$C_p = 0.839 \quad T_a = 536 \quad A_s = 7.876 \quad V_m = 78.231 \quad P_{bar} = 29.13 \quad \sqrt{\Delta P_{avg}} = 0.576$$

$$\theta = \frac{120}{29.24} \quad T_m = 540 \quad A_n = 3.824 \quad \gamma_a = 1.009 \quad P_{stat} = 29.20 \quad \Delta H = 1.448$$

## FROM PHYSICAL SCIENCE:

$$V_{1c} = 46.3 \quad M_n = \quad \%CO_2 = 0.0 \quad \%O_2 = 20.9 \quad \%N_2 = 78.1$$

## PRESSURE CALCULATIONS:

$$P_m = P_{bar} + \frac{\Delta H}{13.6} = ( ) + \frac{( )}{13.6} = 29.24 \text{ in. Hg}$$

$$P_t = P_{bar} + \frac{P_{stat}}{13.6} = ( ) + \frac{( )}{13.6} = 29.14 \text{ in. Hg}$$

## DRY GAS VOLUME:

$$V_{m,d} = \frac{17.65 V_m \gamma_m P_m}{T_m} = \frac{17.65 ( ) ( ) ( )}{( )} = 76.39 \text{ dscf}$$

## MOISTURE CONTENT:

$$B_{wo} = \frac{V_{w,d}}{V_{m,d} + V_{w,d}} = \frac{( )}{( ) + ( )} = 0.028$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

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ISOKINETIC DATA SHEET<sup>1</sup>  
(Continued)

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 3 June 2003

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 1

STACK GAS MOLECULAR WEIGHT:

$$M_s = (1 - B_{wo}) [0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)] + 18B_{wo}$$

$$= (1 - ) [0.44 ( ) + 0.32 ( ) + 0.28 ( )] + 18 ( ) = \underline{28.54} \frac{lb}{lb \text{ mole wet}}$$

STACK GAS VELOCITY:

$$V_{s_{avg}} = 85.48 C_p \sqrt{\Delta P_{avg}} \sqrt{\frac{T_s}{P_s M_s}} = 85.48 ( ) ( ) \sqrt{\frac{( )}{( ) ( )}} = \underline{33.16} \frac{ft}{sec}$$

STACK GAS VOLUMETRIC FLOW RATE:

$$Q_s = \frac{63,529 (1 - B_{wo}) V_{s_{avg}} A_s P_s}{T_s} = \frac{63,529 (1 - ) ( ) ( ) ( )}{( )} = \underline{877,212} \frac{dscf}{hr}$$

PERCENT ISOKINETIC:

$$I = \frac{0.0945 T_s V_{s_{std}}}{\Theta V_s P_s A_n (1 - B_{wo})} = \frac{0.0945 ( ) ( )}{( ) ( ) ( ) ( ) (1 - )} = \underline{101.5} \%$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

FIELD DATA SHEET		RUN NO. 1		DATE 3 JUN 03	
Project Number: 43-EL-5116-03		Installation: Anniston Army Depot, Alabama		Meter Box Operator: Simonevitch	
Sample Location: Chrome Plating Finishing Complex, BLDG 114					
Type of Sample: Total Chrome Moisture					
Nomograph/Calculator		Nozzle		Pitot Tube	
$\Delta H_g$ 1.86	$\Delta P_{avg}$ 0.360	No. 1	$D_g$ 0.249	No. 5-3	$C_p$ 0.84
%H <sub>2</sub> O 1	$P_s/P_m$ 1.0		0.248	F <sub>blockage</sub> 1.411	
$T_a$ 540	$T_s$ 537		0.250	$C_{p,eff}$ 0.84	
"C" Factor	$K_p$ 4.20				
Ref $\Delta P$		$D_{g,avg}$ 0.249		$A_a$ 3.382 x 10 <sup>-7</sup>	
Meter Box No. 90496		Dry Gas Meter $\gamma_a$ 1.009		$D_s$ 38"	$A_s$ 7.876
Filter		Probe			
Type	Number	Length	Liner	Heat Set	
NA	NA	3' EFF	QUARTZ	240	
Initial Leak Check		Initial Pitot Tube Leak Check			
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
15	0.001 ft <sup>3</sup> per 1 Min.	at 5.8 / 6.3 in. H <sub>2</sub> O			
Final Leak Check		Final Pitot Tube Leak Check			
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
5	0.001 ft <sup>3</sup> per 1 Min.	at 5.3 / 5.7 in. H <sub>2</sub> O			
Gas Bag System Leak Check		Component Leak Check			
Initial	Final	Vacuum (in. Hg.)	Leak Rate		
$P_{bar}$ 29.13	$P_{stat}$ +0.20		ft <sup>3</sup> per Min.		
Start Time 1115	End Time 1125		ft <sup>3</sup> per Min.		

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Point No.	$\theta$ (min)	$V_n$ (ft <sup>3</sup> ) $V_t =$	$\Delta P$ ("H <sub>2</sub> O)	$(\Delta P)^{1/2}$	$\Delta H$ ("H <sub>2</sub> O)	$T_n$ (°F) $t_i$ $t_f$	$T_s$ (°F)	Vacuum ("Hg)	Final Imp. Temp. (°F)	Filter Temp. (°F)	Remark
		394.793									4.20
1	5	378.23	0.38	0.616	1.60	71 72	74	2.0	53	-	240
2	10	401.67	0.38	0.616	1.60	77 72	76	2.0	52	-	241
3	15	404.99	0.39	0.625	1.51	76 72	76	2.0	55	-	245
4	20	408.18	0.34	0.533	1.43	76 72	76	2.0	56	-	251
5	25	411.51	0.35	0.592	1.47	76 72	75	2.0	58	-	243
6	30	414.83	0.34	0.533	1.43	83 73	76	2.0	59	-	240
7	35	418.13	0.34	0.533	1.43	84 73	76	2.0	58	-	238
8	40	421.47	0.33	0.574	1.39	83 72	76	2.0	57	-	245
9	45	424.65	0.31	0.557	1.30	86 74	76	1.5	60	-	247
10	50	428.35	0.42	0.648	1.76	86 75	76	2.0	58	-	239
11	55	432.37	0.47	0.686	1.97	88 75	77	2.5	58	-	250
12	60	436.150	0.47	0.686	1.97	89 76	77	2.5	58	-	246
		436.151									
13	65	439.46	0.33	0.574	1.39	76 77	76	1.5	59	-	250
14	70	442.58	0.32	0.566	1.39	84 77	76	1.5	50	-	245
15	75	445.85	0.32	0.566	1.34	86 77	77	1.5	52	-	-
16	80	448.75	0.29	0.539	1.218	85 77	76	1.5	52	-	-
17	85	451.92	0.29	0.539	1.218	88 78	77	1.5	55	-	-
18	90	454.90	0.28	0.529	1.176	88 78	77	1.5	59	-	-
19	95	457.97	0.28	0.529	1.176	88 78	77	1.5	55	-	-
20	100	461.13	0.34	0.533	1.43	88 79	77	1.5	56	-	-
21	105	464.43	0.33	0.574	1.39	89 79	77	1.5	55	-	-
22	110	467.73	0.34	0.533	1.43	81 79	77	1.5	55	-	-
23	115	470.83	0.33	0.574	1.39	90 80	77	1.5	56	-	-
24	120	474.024	0.33	0.574	1.39	89 80	77	1.5	56	-	-
TOTAL		79.251	0.530	1.821	24.748	26.793	175				
		AVERAGE		0.576	1.448	68.288	76 °F				
						540 °R	536 °R				

START 1115      STOP 1237  
 START 1215      STOP 1337

MID PT CK AREA 0.005 AWP/min @ 3" Hg



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

# ISOKINETIC DATA SHEET<sup>1</sup>

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 3 June 2003

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 2

## FROM FIELD DATA SHEET:

$$C_p = 0.839 \quad T_s = 537 \quad A_s = 7.876 \quad V_m = 78.076 \quad P_{bar} = 29.13 \quad \sqrt{\Delta P_{avg}} = 0.577$$

$$\theta = 12.0 \quad T_m = 545 \quad A_n = 3.3828 \times 10^{-4} \quad \gamma_n = 1.009 \quad P_{stat} = 29.20 \quad \Delta H = 0.4140$$

## FROM PHYSICAL SCIENCE:

$$V_{lc} = 48.1 \quad M_n = \quad \%CO_2 = 0.0 \quad \%O_2 = 20.9 \quad \%N_2 = 79.1$$

## PRESSURE CALCULATIONS:

$$P_m = P_{bar} + \frac{\Delta H}{13.6} = ( ) + \frac{( )}{13.6} = 29.23 \text{ in. Hg}$$

$$P_s = P_{bar} + \frac{P_{stat}}{13.6} = ( ) + \frac{( )}{13.6} = 29.14 \text{ in. Hg}$$

## DRY GAS VOLUME:

$$V_{m,d} = \frac{17.65 V_m \gamma_m P_m}{T_m} = \frac{17.65 ( ) ( ) ( )}{( )} = 74.58 \text{ dscf}$$

## MOISTURE CONTENT:

$$B_{wv} = \frac{V_{w,d}}{V_{m,d} + V_{w,d}} = \frac{( )}{( ) + ( )} = 0.030$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>  
(Continued)

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 3 June  
LOCATION: Chrome Plating Finishing Complex, BLDG 114 RUN NUMBER: 2

STACK GAS MOLECULAR WEIGHT:

$$M_s = (1 - B_{wo}) [0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)] + 18B_{wo}$$

$$= (1 - ) [0.44 ( ) + 0.32 ( ) + 0.28 ( )] + 18 ( ) = \underline{28.52} \frac{lb}{lb \text{ mole wet}}$$

STACK GAS VELOCITY:

$$V_{s_{avg}} = 85.48 C_p \sqrt{\Delta P_{avg}} \sqrt{\frac{T_s}{P_s M_s}} = 85.48 ( ) ( ) \sqrt{\frac{( )}{( ) ( )}} = \underline{31.52} \frac{ft}{sec}$$

STACK GAS VOLUMETRIC FLOW RATE:

$$Q_s = \frac{63,529 (1 - B_{wo}) V_{s_{avg}} A_s P_s}{T_s} = \frac{63,529 (1 - ) ( ) ( ) ( )}{( )} = \underline{876.646} \frac{dscf}{hr}$$

PERCENT ISOKINETIC:

$$I = \frac{0.0945 T_s V_{s_{avg}}}{\Theta V_s P_s A_s (1 - B_{wo})} = \frac{0.0945 ( ) ( )}{( ) ( ) ( ) ( ) (1 - )} = \underline{99.1} \%$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

FIELD DATA SHEET		RUN NO. 2		DATE 3 June 2003	
Project Number: 43-EL-5116-03		Installation: Anniston Army Depot, Alabama		Meter Box Operator: Simeonovitch	
Sample Location: Chrome Plating Finishing Complex, BLDG 114					
Type of Sample: <u>Total Chrome</u> <u>Moisture</u>					
Nomograph/Calculator		Nozzle		Pitot Tube	
$\Delta H_a$ 1.86	$\Delta P_{avg}$ 0.366	No.	$D_a$	No.	$C_p$
%H <sub>2</sub> O 1	$P_s/P_a$ 1.0	N-1	0.249	5.3	0.84
$T_a$ 540	$T_s$ 537		0.248	$F_{blockage}$ 1.411	
"C" Factor	$K_p$ 4.26		0.250	$C_{p,eff}$ 0.84	
Ref. $\Delta P$		$D_{n,avg}$	0.249	$A_n$ $3.382 \times 10^{-4}$	
Meter Box No. 90496		Dry Gas Meter $\gamma_m$	1.009	$D_s$ 38"	$A_s$ 7.876
Filter			Probe		
Type	Number	Length	Liner	Heat Set	
		3' Eff	Alum. V2		
Initial Leak Check			Initial Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
15	0.001 ft <sup>3</sup> per 1 Min.	at 6.3 / 6.1 in. H <sub>2</sub> O			
Final Leak Check			Final Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
5	0.001 ft <sup>3</sup> per 1 Min.	at 7.1 / 6.5 in. H <sub>2</sub> O			
Gas Bag System Leak Check			Component Leak Check		
Initial	Final	Vacuum (in. Hg.)	Leak Rate		
$P_{bar}$ 29.13	$P_{stat}$ +0.20		ft <sup>3</sup> per Min.		
Start Time 1425	End Time 1635		ft <sup>3</sup> per Min.		

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

Point No.	$\Theta$ (min)	$V_m$ (ft <sup>3</sup> ) $V_1 =$	$\Delta P$ ("H <sub>2</sub> O)	$(\Delta P)^{1/2}$	$\Delta H$ ("H <sub>2</sub> O)	$T_a$ (°F) $t_i$ $t_f$		$T_a$ (°F)	Vacuum ("Hg)	Final Imp. Temp. (°F)	Filter Temp. (°F)	Remark $K_p =$
		474.243										4.20
1	5	477.55	0.35	0.592	1.47	75	76	75	2.0	63	-	4.20
2	10	480.88	0.36	0.600	1.51	80	77	77	2.0	61	-	4.20
3	15	484.19	0.35	0.592	1.47	83	76	76	2.0	55	-	4.20
4	20	487.45	0.30	0.549	1.26	86	77	76	2.0	58	-	4.20
5	25	490.51	0.31	0.557	1.30	87	77	76	1.5	55	-	4.20
6	30	493.43	0.27	0.520	1.13	88	78	76	1.5	58	-	4.20
7	35	496.36	0.26	0.510	1.09	88	78	76	1.5	56	-	4.20
8	40	499.33	0.30	0.548	1.26	88	78	77	1.5	55	-	4.20
9	45	502.57	0.31	0.557	1.30	89	78	77	1.5	55	-	4.20
10	50	505.63	0.31	0.557	1.30	90	79	77	1.5	54	-	4.20
11	55	508.83	0.32	0.566	1.34	91	79	77	1.5	55	-	4.20
12	60	512.180	0.33	0.574	1.39	91	80	77	1.5	56	-	4.20
13	65	515.59	0.39	0.624	1.64	84	81	77	2.0	58	-	4.20
14	70	519.09	0.38	0.616	1.60	87	80	77	2.0	53	-	4.20
15	75	522.61	0.39	0.624	1.64	91	81	77	2.0	54	-	4.20
16	80	525.66	0.28	0.529	1.18	92	81	78	1.5	55	-	4.20
17	85	528.75	0.28	0.529	1.18	92	82	78	1.5	56	-	4.20
18	90	531.96	0.26	0.510	1.09	93	82	78	1.5	56	-	4.20
19	95	534.71	0.31	0.557	1.30	93	82	78	1.5	55	-	4.20
20	100	537.98	0.31	0.557	1.30	94	83	78	1.5	56	-	4.20
21	105	541.10	0.32	0.566	1.34	96	84	79	1.5	56	-	4.20
22	110	544.81	0.44	0.667	1.85	95	84	78	2.0	56	-	4.20
23	115	548.53	0.44	0.663	1.85	94	85	78	2.0	58	-	4.20
24	120	552.319	0.43	0.656	1.81	94	85	78	2.0	58	-	4.20
TOTAL		78.076		13.841	33.60	4064		1851				
AVERAGE				0.577	1.40	85 °F		77 °F				
						545 °R		637 °R				

Start 1425      Stop 1528  
 Start 1528      Stop 1628

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 3 June

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 3

FROM FIELD DATA SHEET:

$C_p = 0.839$   $T_s = 544$   $A_s = 7.876$   $V_m = 77.904$   $P_{bar} = 29.11$   $\sqrt{\Delta P_{avg}} = 0.545$   
 $\theta = 120$   $T_m = 544$   $A_n = 3.582 \times 10^{-4}$   $\gamma_a = 1.009$   $P_{stat} = 0.20$   $\Delta H = 1.361$

FROM PHYSICAL SCIENCE:

$V_{1c} = 47.7$   $M_a = \underline{\hspace{1cm}}$   $\%CO_2 = 0.0$   $\%O_2 = 20.9$   $\%N_2 = 79.1$

PRESSURE CALCULATIONS:

$$P_m = P_{bar} + \frac{\Delta H}{13.6} = ( ) + \frac{( )}{13.6} = 29.23 \text{ in. Hg}$$

$$P_s = P_{bar} + \frac{P_{stat}}{13.6} = ( ) + \frac{( )}{13.6} = 29.14 \text{ in. Hg}$$

DRY GAS VOLUME:

$$V_{m_{nd}} = \frac{17.65 V_m \gamma_m P_m}{T_m} = \frac{17.65 ( ) ( ) ( )}{( )} = 73.87 \text{ dscf}$$

MOISTURE CONTENT:

$$B_{wo} = \frac{V_{w_{nd}}}{V_{m_{nd}} + V_{w_{nd}}} = \frac{( )}{( ) + ( )} = 0.030$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>  
(Continued)

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 3 June 2003

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 3

STACK GAS MOLECULAR WEIGHT:

$$M_s = (1 - B_{wo}) [0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)] + 18B_{wo}$$

$$= (1 - ) [0.44 ( ) + 0.32 ( ) + 0.28 ( )] + 18 ( ) = \underline{28.52} \frac{lb}{lb \text{ mole wet}}$$

STACK GAS VELOCITY:

$$V_{s,ave} = 85.48 C_p \sqrt{\Delta P_{avg}} \sqrt{\frac{T_s}{P_s M_s}} = 85.48 ( ) ( ) \sqrt{\frac{( )}{( ) ( )}} = \underline{31.57} \frac{ft}{sec}$$

STACK GAS VOLUMETRIC FLOW RATE:

$$Q_s = \frac{63,529 (1 - B_{wo}) V_{s,ave} A_s P_s}{T_s} = \frac{63,529 (1 - ) ( ) ( ) ( )}{( )} = \underline{825,699} \frac{dscf}{hr}$$

PERCENT ISOKINETIC:

$$I = \frac{0.0945 T_s V_{s,ave}}{\Theta V_s P_s A_n (1 - B_{wo})} = \frac{0.0945 ( ) ( )}{( ) ( ) ( ) ( ) (1 - )} = \underline{104.2} \%$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

FIELD DATA SHEET		RUN NO. 3		DATE 3 June 2003	
Project Number: 43-EL-5116-03		Installation: Anniston Army Depot, Alabama		Meter Box Operator: Simonevich	
Sample Location: Chrome Plating Finishing Complex, BLDG 114					
Type of Sample: Total Chrome Moisture					
Nomograph/Calculator		Nozzle		Pitot Tube	
$\Delta H_0$ 1.86	$\Delta P_{avg}$ 0.36	No.	$D_n$	No.	$C_p$
%H <sub>2</sub> O 1	$P_0/P_n$ 1.0	N-1	0.249	5-3	0.84
$T_n$ 540	$T_s$ 537	↓	0.248	$F_{blockage}$ 1.411	
"C" Factor	$K_p$ 4.20	↓	0.250	$C_{p,eff}$ 0.84	
Ref $\Delta P$		$D_{n,avg}$	0.249	$A_n$ 3.382 $\times 10^{-4}$	
Meter Box No. 90496		Dry Gas Meter $\gamma_n$	1.019	$D_s$ 38"	$A_s$ 7.876
Filter			Probe		
Type	Number	Length	Liner	Heat Set	
		3' E 8"	Quartz		
Initial Leak Check			Initial Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
0.003 15"	0.003 ft <sup>3</sup> per 1 Min.	at 6.5 / 7.2 in. H <sub>2</sub> O			
Final Leak Check			Final Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
5"	0.001 ft <sup>3</sup> per 1 Min.	at 7.3 / 7.1 in. H <sub>2</sub> O			
Gas Bag System Leak Check			Component Leak Check		
Initial	Final	Vacuum (in Hg.)	Leak Rate		
$P_{bar}$ 29.13	$P_{stat}$ 29.20		ft <sup>3</sup> per Min.		
Start Time 1700	End Time 1910		ft <sup>3</sup> per Min.		

## Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

Point No.	Θ (min)	V <sub>m</sub> (ft <sup>3</sup> ) V <sub>i</sub> =	ΔP ("H <sub>2</sub> O)	(ΔP) <sup>1/2</sup>	ΔH ("H <sub>2</sub> O)	T <sub>a</sub> (°F) t <sub>i</sub> t <sub>f</sub>		T <sub>a</sub> (°F)	Vacuum ("Hg)	Final Imp. Temp. (°F)	Filter Temp. (°F)	Remark K <sub>p</sub> =
		552.581										4.20
1	5	556.14	0.42	0.648	1.76	80	81	78	2.0	63	63	4.20
2	10	559.87	0.41	0.640	1.72	85	81	79	2.0	53	-	4.20
3	15	563.40	0.42	0.648	1.76	91	82	79	2.0	52	-	4.20
4	20	566.97	0.37	0.608	1.55	94	83	80	2.0	52	-	4.20
5	25	570.48	0.38	0.616	1.60	94	83	80	2.0	52	-	4.20
6	30	573.47	0.28	0.529	1.18	94	83	80	1.5	52	-	4.20
7	35	576.50	0.28	0.529	1.18	95	84	80	1.5	52	-	4.20
8	40	579.47	0.27	0.520	1.13	95	84	80	1.5	52	-	4.20
9	45	582.51	0.28	0.529	1.18	97	85	80	1.5	54	-	4.20
10	50	585.71	0.30	0.548	1.26	95	85	79	1.5	51	-	4.20
11	55	589.10	0.35	0.592	1.47	95	85	79	1.5	53	-	4.20
12	60	592.580	0.35	0.592	1.47	96	85	79	1.5	52	-	4.20
13	65	595.67	0.31	0.548	1.30	90	85	79	1.5	56	-	4.20
14	70	598.93	0.32	0.566	1.34	94	86	80	1.5	57	-	4.20
15	75	602.14	0.32	0.566	1.34	94	85	80	1.5	52	-	4.20
16	80	605.44	0.31	0.548	1.30	95	86	80	1.5	53	-	4.20
17	85	608.68	0.32	0.566	1.34	96	86	80	1.5	54	-	4.20
18	90	611.52	0.26	0.509	1.10	96	86	80	1.5	54	-	4.20
19	95	614.51	0.27	0.520	1.13	95	85	80	1.5	54	-	4.20
20	100	617.64	0.29	0.539	1.22	95	86	80	1.5	55	-	4.20
21	105	620.89	0.32	0.566	1.34	96	86	80	1.5	53	-	4.20
22	110	624.11	0.33	0.574	1.39	96	86	80	1.5	54	-	4.20
23	115	627.29	0.31	0.548	1.30	96	86	80	1.5	53	-	4.20
24	120	630.485	0.31	0.548	1.30	95	86	80	1.5	54	-	4.20
TOTAL		77.904		13.068	32.66	4279	1912					
AVERAGE				0.545	1.361	89 °F	80 °F					
						549 °R	540 °R					

START 1700

START 1840

STOP 1800

STOP 1910



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

# ISOKINETIC DATA SHEET<sup>1</sup>

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 4 June 2003

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 4

## FROM FIELD DATA SHEET:

$$C_p = \underline{0.839} \quad T_a = \underline{537} \quad A_a = \underline{7.876} \quad v_a = \underline{84.318} \quad P_{bar} = \underline{29.19} \quad \sqrt{\Delta P_{avg}} = \underline{0.621}$$

$$\theta = \underline{124} \quad T_n = \underline{556} \quad A_n = \underline{3.382} \quad \gamma_m = \underline{1.009} \quad P_{stat} = \underline{29.20} \quad \Delta H = \underline{1.62}$$

## FROM PHYSICAL SCIENCE:

$$V_{lc} = \underline{32.6} \quad M_n = \underline{\quad} \quad \%CO_2 = \underline{0.0} \quad \%O_2 = \underline{20.9} \quad \%N_2 = \underline{79.1}$$

## PRESSURE CALCULATIONS:

$$P_m = P_{bar} + \frac{\Delta H}{13.6} = ( \quad ) + \frac{( \quad )}{13.6} = \underline{29.31} \text{ in. Hg}$$

$$P_s = P_{bar} + \frac{P_{stat}}{13.6} = ( \quad ) + \frac{( \quad )}{13.6} = \underline{29.20} \text{ in. Hg}$$

## DRY GAS VOLUME:

$$V_{mnd} = \frac{17.65 V_m \gamma_m P_m}{T_m} = \frac{17.65 ( \quad ) ( \quad ) ( \quad )}{( \quad )} = \underline{79.16} \text{ dscf}$$

## MOISTURE CONTENT:

$$B_{wg} = \frac{V_{wgd}}{V_{mnd} + V_{wgd}} = \frac{( \quad )}{( \quad ) + ( \quad )} = \underline{0.019}$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>  
(Continued)

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 4 June 2003

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 4

STACK GAS MOLECULAR WEIGHT:

$$M_s = (1 - B_{wo}) [0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)] + 18B_{wo}$$

$$= (1 - ) [0.44 ( ) + 0.32 ( ) + 0.28 ( )] + 18 ( ) = \underline{28.63} \frac{lb}{lb \text{ mole wet}}$$

STACK GAS VELOCITY:

$$V_{s,avg} = 85.48 C_p \sqrt{\Delta P_{avg}} \sqrt{\frac{T_s}{P_s M_s}} = 85.48 ( ) ( ) \sqrt{\frac{( )}{( ) ( )}} = \underline{36.69} \frac{ft}{sec}$$

STACK GAS VOLUMETRIC FLOW RATE:

$$Q_s = \frac{63,529 (1 - B_{wo}) V_{s,avg} A_s P_s}{T_s} = \frac{63,529 (1 - ) ( ) ( ) ( )}{( )} = \underline{953,772} \frac{dscf}{hr}$$

PERCENT ISOKINETIC:

$$I = \frac{0.0945 T_s V_{s,avg}}{\ominus V_s P_s A_n (1 - B_{wo})} = \frac{0.0945 ( ) ( )}{( ) ( ) ( ) ( ) (1 - )} = \underline{96.8} \%$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

## Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

FIELD DATA SHEET		RUN NO. 4		DATE 4 June 2003	
Project Number: 43-EL-5116-03		Installation: Anniston Army Depot, Alabama		Meter Box Operator: Simenovich	
Sample Location: Chrome Plating Finishing Complex, BLDG 114					
Type of Sample: Total Chrome Moisture					
Nomograph/Calculator		Nozzle		Pitot Tube	
$\Delta H_s$ 1.86	$\Delta P_{avg}$ 0.36	No.	$D_n$	No.	$C_p$
%H <sub>2</sub> O 2	$P_s/P_m$ 1.0	N-1	0.249	5-3	0.84
$T_a$ 545	$T_s$ 537	↓	0.248	$F_{blockage}$ 1.411	
"C" Factor	$K_p$ 4.16		0.250	$C_{p,eff}$ 0.84	
Ref $\Delta P$		$D_{n,avg}$ 0.249		$A_n$ 3.382 x 10 <sup>-4</sup>	
Meter Box No. 90489 <sup>96</sup>		Dry Gas Meter $\gamma_m$ 1.009		$D_s$ 3"	$A_s$ 7.871
Filter			Probe		
Type	Number	Length	Liner	Heat Set	
NA	NA	3' EST	Quartz	—	
Initial Leak Check			Initial Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
15	0.001 ft <sup>3</sup> per 1 Min.	at 6.5 / 7.3 in. H <sub>2</sub> O			
Final Leak Check			Final Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
2.5	0.001 ft <sup>3</sup> per 1 Min.	at 6.2 / 6.8 in. H <sub>2</sub> O			
Gas Bag System Leak Check			Component Leak Check		
Initial	Final	Vacuum (in. Hg.)	Leak Rate		
$P_{bar}$ 29.19	$P_{stat}$ 10.20		ft <sup>3</sup> per Min.		
Start Time 0820	End Time 1030		ft <sup>3</sup> per Min.		

## Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

Point No.	$\theta$ (min)	$V_n$ (ft <sup>3</sup> ) $V_1 =$	$\Delta P$ ("H <sub>2</sub> O)	$(\Delta P)^{1/2}$	$\Delta H$ ("H <sub>2</sub> O)	$T_n$ (°F) $t_1$ $t_2$	$T_o$ (°F)	Vacuum ("Hg)	Final Imp. Temp. (°F)	Filter Temp. (°F)	Remark $K_p =$
		630.644									4.16
1	5	634.08	0.38	0.616	1.58	81 80	78	1.5	55	5	4.16
2	10	637.42	0.37	0.608	1.54	81 80	78	1.5	54	-	4.16
3	15	640.77	0.37	0.608	1.54	85 81	77	1.5	52	-	4.16
4	20	644.12	0.39	0.624	1.62	89 82	77	1.5	54	-	4.16
5	25	647.24	0.30	0.548	1.25	94 86	77	1.5	59	-	4.16
6	30	650.32	0.29	0.539	1.20	96 87	77	1.5	58	-	4.16
7	35	653.41	0.30	0.547	1.25	99 89	77	1.5	59	-	4.16
8	40	656.75	0.33	0.574	1.37	100 90	77	1.5	56	-	4.16
9	45	660.02	0.34	0.583	1.41	100 92	77	1.5	55	-	4.16
10	50	663.53	0.39	0.624	1.62	101 97	77	1.5	53	-	4.16
11	55	667.02	0.38	0.616	1.58	103 94	77	1.5	53	-	4.16
12	60	670.52	0.37	0.608	1.54	103 95	77	1.5	55	-	4.16
13	65	674.15	0.42	0.648	1.75	100 97	77	2.0	55	-	4.16
14	70	677.99	0.44	0.663	1.83	101 98	77	2.0	54	-	4.16
15	75	681.65	0.41	0.640	1.71	103 99	77	2.0	55	-	4.16
16	80	685.40	0.42	0.648	1.75	103 99	77	2.0	53	-	4.16
17	85	689.08	0.41	0.640	1.71	104 100	77	2.0	54	-	4.16
18	90	692.57	0.39	0.624	1.62	104 100	76	2.0	56	-	4.16
19	95	695.71	0.29	0.539	1.20	103 100	77	1.5	54	-	4.16
20	100	699.10	0.37	0.608	1.54	103 100	76	1.5	55	-	4.16
21	105	702.81	0.44	0.663	1.83	101 100	76	2.0	58	-	4.16
22	110	706.91	0.53	0.728	2.21	103 101	77	2.5	57	-	4.16
23	115	710.92	0.50	0.707	2.08	105 101	77	2.5	56	-	4.16
24	120	714.962	0.50	0.707	2.08	105 101	77	2.5	54	-	4.16
TOTAL		843.18	9.72	14.91	38.81	4612	1847				
AVERAGE			0.405	0.621	1.62	96 °F	77 °F				
						556 °R	537 °R				

SMF 0825

SMF 0930

SP01 0925

SP01 1030



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 6/4/03  
LOCATION: Chrome Plating Finishing Complex, BLDG 114 RUN NUMBER: 5

FROM FIELD DATA SHEET:

$C_p = 0.839$   $T_s = 540$   $A_s = 7.876$   $V_s = 82.512$   $P_{bar} = 29.19$   $\sqrt{\Delta P_{avg}} = 0.600$   
 $\theta = 120$   $T_m = 560$   $A_m = 3.282 \times 10^{-4}$   $\gamma_m = 1.009$   $P_{stat} = 0.20$   $\Delta H = 1.54$

FROM PHYSICAL SCIENCE:

$V_{1c} = 34.7$   $M_n =$   $\%CO_2 = 0.0$   $\%O_2 = 20.9$   $\%N_2 = 79.1$

PRESSURE CALCULATIONS:

$$P_m = P_{bar} + \frac{\Delta H}{13.6} = ( ) + \frac{( )}{13.6} = 29.30 \text{ in. Hg}$$

$$P_s = P_{bar} + \frac{P_{stat}}{13.6} = ( ) + \frac{( )}{13.6} = 29.20 \text{ in. Hg}$$

DRY GAS VOLUME:

$$V_{m,d} = \frac{17.65 V_m \gamma_m P_m}{T_m} = \frac{17.65 ( ) ( ) ( )}{( )} = 76.80 \text{ dscf}$$

MOISTURE CONTENT:

$$B_{wo} = \frac{V_{w,d}}{V_{m,d} + V_{w,d}} = \frac{( )}{( ) + ( )} = 0.021$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>  
(Continued)

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 6/4/03

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 5

STACK GAS MOLECULAR WEIGHT:

$$M_s = (1 - B_{wo}) [0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)] + 18B_{wo}$$

$$= (1 - ) [0.44 ( ) + 0.32 ( ) + 0.28 ( )] + 18 ( ) = \underline{28.61} \frac{lb}{lb \text{ mole wet}}$$

STACK GAS VELOCITY:

$$V_{s,avg} = 85.48 C_p \sqrt{\Delta P_{avg}} \sqrt{\frac{T_s}{P_s M_s}} = 85.48 ( ) ( ) \sqrt{\frac{( )}{( ) ( )}} = \underline{34.59} \frac{ft}{sec}$$

STACK GAS VOLUMETRIC FLOW RATE:

$$Q_s = \frac{63,529 (1 - B_{wo}) V_{s,avg} A_s P_s}{T_s} = \frac{63,529 (1 - ) ( ) ( ) ( )}{( )} = \underline{916,783} \frac{dscf}{hr}$$

PERCENT ISOKINETIC:

$$I = \frac{0.0945 T_s V_{s,avg}}{\Theta V_s P_s A_s (1 - B_{wo})} = \frac{0.0945 ( ) ( )}{( ) ( ) ( ) ( ) (1 - )} = \underline{97.7} \%$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

FIELD DATA SHEET		RUN NO. 5		DATE 4 Jun 2003	
Project Number: 43-EL-5116-03		Installation: Anniston Army Depot, Alabama		Meter Box Operator: S. Kovitch	
Sample Location: Chrome Plating Finishing Complex, BLDG 114					
Type of Sample: Total Chrome Moisture					
Nomograph/Calculator		Nozzle		Pitot Tube	
$\Delta H_s$ 1.86	$\Delta P_{avg}$ 0.36	No. 1	$D_n$ 0.249	No. 0.853	$C_p$ 0.84
%H <sub>2</sub> O 2	$P_s/P_a$ 1.0		0.249		
$T_n$ 546	$T_a$ 537		0.249	$F_{blockage}$ 1.411	
"C" Factor	$K_p$ 4.19 4.21		0.250	$C_{p, eff}$	
Ref $\Delta P$		$D_{n, avg}$ 0.249		$A_n$ 3.382 x 10 <sup>-4</sup>	
Meter Box No. 9048		Dry Gas Meter $\gamma$ 1.009		$D_s$ 38"	$A_s$ 7.876
Filter			Probe		
Type	Number	Length	Liner	Heat Set	
NA	NA	3' E82	Quartz		
Initial Leak Check			Initial Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate		0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.		
15"	0.003 ft <sup>3</sup> per 1 Min.		at 7.5 / 6.8 in. H <sub>2</sub> O		
Final Leak Check			Final Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate		0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.		
20"	0.001 ft <sup>3</sup> per 1 Min.		at 7.1 / 7.2 in. H <sub>2</sub> O		
Gas Bag System Leak Check			Component Leak Check		
Initial	Final	Vacuum (in Hg.)	Leak Rate		
$P_{bar}$ 29.19	$P_{stat} + 0.20$		ft <sup>3</sup> per Min.		
Start Time 1100	End Time 1305		ft <sup>3</sup> per Min.		



## Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

Point No.	Θ (min)	V <sub>a</sub> (ft <sup>3</sup> ) V <sub>i</sub>	ΔP ("H <sub>2</sub> O)	(ΔP) <sup>1/2</sup>	ΔH ("H <sub>2</sub> O)	T <sub>a</sub> (°F) t <sub>i</sub> t <sub>e</sub>		T <sub>s</sub> (°F)	Vacuum ("Hg)	Final Imp. Temp. (°F)	Filter Temp. (°F)	Remark
		715.286										4.25 K <sub>p</sub> = 104 4.25
1	5	719.30	0.44	0.663	1.87	96	101	78	2.5	65	-	4.19 4.25
2	10	722.89	0.45	0.671	1.89	96	101	78	2.5	62	-	4.19 4.25
3	15	726.87	0.45	0.671	1.89	102	101	78	2.5	49	-	4.19 4.25
4	20	730.66	0.44	0.663	1.87	101	99	78	2.5	46	-	4.19 4.25
5	25	733.97	0.32	0.566	1.36	100	99	78	1.5	45	-	4.19 4.25
6	30	736.99	0.32	0.566	1.36	101	100	78	1.5	46	-	4.19 4.25
7	35	740.46	0.27	0.520	1.14	102	99	79	1.5	47	-	4.19 4.25
8	40	743.28	0.26	0.509	1.11	102	99	80	1.5	45	-	4.19 4.25
9	45	746.36	0.28	0.529	1.19	102	99	81	1.5	43	-	4.19 4.25
10	50	749.46	0.30	0.548	1.28	103	99	81	1.5	46	-	4.19 4.25
11	55	752.75	0.34	0.583	1.45	105	100	82	2.0	50	-	4.19 4.25
12	60	756.053	0.34	0.583	1.45	105	99	82	2.0	51	-	4.19 4.25
13	65	759.59	0.37	0.608	1.57	99	99	81	2.0	55	-	4.19 4.25
14	70	763.13	0.59	0.625	1.66	99	98	81	2.0	47	-	4.19 .5
15	75	766.81	0.40	0.632	1.70	100	98	81	2.0	46	-	4.19 4.25
16	80	770.36	0.39	0.625	1.66	102	98	81	2.0	50	-	4.19 4.25
17	85	773.49	0.30	0.548	1.28	102	98	82	1.5	47	-	4.19 4.25
18	90	776.51	0.28	0.529	1.19	102	97	82	1.5	49	-	4.19 4.25
19	95	779.65	0.30	0.548	1.28	104	97	82	1.5	48	-	4.19 4.25
20	100	783.05	0.38	0.616	1.62	106	98	82	2.0	49	-	4.19 4.25
21	105	786.44	0.36	0.606	1.53	103	97	81	2.0	48	-	4.19 4.25
22	110	790.22	0.45	0.671	1.91	104	97	81	2.0	49	-	4.19 4.25
23	115	794.01	0.44	0.663	1.87	105	98	81	2.0	50	-	4.19 4.25
24	120	797.898	0.44	0.663	1.87	106	98	81	2.0	49	-	4.19 4.25
TOTAL		82512	8.71	14.400	37.04	4816		1929				
AVERAGE			0.36	0.600	1.54	100 °F		80 °F				
						560 °R		540 °R				

START 1106 1205

STOP 1200 1305



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 4 June 2003

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 6

FROM FIELD DATA SHEET:

$$C_p = 0.839 \quad T_a = 544 \quad A_a = 7.876 \quad V_m = 80.795 \quad P_{bar} = 29.18 \quad \sqrt{\Delta P_{avg}} = 0.586$$

$$\theta = 120 \quad T_m = 560 \quad A_m = 3.312 \times 10^{-4} \quad \gamma_a = 1.009 \quad P_{stat} = 0.20 \quad \Delta H = 1.47$$

FROM PHYSICAL SCIENCE:

$$V_{ic} = 34.5 \quad M_n = \quad \%CO_2 = 0.0 \quad \%O_2 = 20.9 \quad \%N_2 = 79.1$$

PRESSURE CALCULATIONS:

$$P_m = P_{bar} + \frac{\Delta H}{13.6} = ( ) + \frac{( )}{13.6} = 29.36 \text{ in. Hg}$$

$$P_s = P_{bar} + \frac{P_{stat}}{13.6} = ( ) + \frac{( )}{13.6} = 29.26 \text{ in. Hg}$$

DRY GAS VOLUME:

$$V_{std} = \frac{17.65 V_m \gamma_m P_m}{T_m} = \frac{17.65 ( ) ( ) ( )}{( )} = 75.28 \text{ dscf}$$

MOISTURE CONTENT:

$$B_{wp} = \frac{V_{w,ad}}{V_{m,ad} + V_{w,ad}} = \frac{( )}{( ) + ( )} = 0.021$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>  
(Continued)

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 4 June 2003

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 6

STACK GAS MOLECULAR WEIGHT:

$$M_s = (1 - B_{wo}) [0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)] + 18B_{wo}$$

$$= (1 - ) [0.44 ( ) + 0.32 ( ) + 0.28 ( )] + 18 ( ) = \underline{28.61} \frac{lb}{lb \text{ mole wet}}$$

STACK GAS VELOCITY:

$$V_{s_{wet}} = 85.48 C_p \sqrt{\Delta P_{avg}} \sqrt{\frac{T_s}{P_s M_s}} = 85.48 ( ) ( ) \sqrt{\frac{( )}{( ) ( )}} = \underline{33.91} \frac{ft}{sec}$$

STACK GAS VOLUMETRIC FLOW RATE:

$$Q_s = \frac{63,529 (1 - B_{wo}) V_{s_{wet}} A_s P_s}{T_s} = \frac{63,529 (1 - ) ( ) ( ) ( )}{( )} = \underline{891,684} \frac{dscf}{hr}$$

PERCENT ISOKINETIC:

$$I = \frac{0.0945 T_s V_{s_{wet}}}{\Theta V_s P_s A_s (1 - B_{wo})} = \frac{0.0945 ( ) ( )}{( ) ( ) ( ) ( ) (1 - )} = \underline{98.4} \%$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

## Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

FIELD DATA SHEET		RUN NO. 6		DATE 4 June 2003	
Project Number: 43-EL-5116-03		Installation: Anniston Army Depot, Alabama		Meter Box Operator: S. Monrovia	
Sample Location: Chrome Plating Finishing Complex, BLDG 114					
Type of Sample: Total Chrome Moisture					
Nomograph/Calculator		Nozzle		Pitot Tube	
$\Delta H_a$ 1.86	$\Delta P_{avg}$ 0.36	No.	$D_n$	No.	$C_p$
%H <sub>2</sub> O 2	$P_a/P_s$ 1.0	N-1	0.249	5-3	0.84
$T_n$ 545	$T_s$ 537	↓	0.248	$F_{blockage}$ 1.411	
"C" Factor	$K_p$ 426		0.250	$C_{p, eff}$	
Ref $\Delta P$		$D_{n, avg}$ 0.249		$A_n$ 3.382 x 10 <sup>-2</sup>	
Meter Box No. 90496		Dry Gas Meter $\gamma_n$ 1.019		$D_s$ 38"	$A_s$ 7.876
Filter			Probe		
Type	Number		Length	Liner	Heat Set
NA	NA		3' E68	Quartz	—
Initial Leak Check			Initial Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate		0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.		
15"	0.004 ft <sup>3</sup> per 1 Min.		at 7.1 / 6.8 in. H <sub>2</sub> O		
Final Leak Check			Final Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate		0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.		
5"	0.002 ft <sup>3</sup> per 1 Min.		at 7.3 / 7.4 in. H <sub>2</sub> O		
Gas Bag System Leak Check			Component Leak Check		
Initial	Final	Vacuum (in. Hg.)	Leak Rate		
$P_{bar}$ 29.19	$P_{stat}$ 0.20		ft <sup>3</sup> per Min.		
Start Time 1330	End Time 1533		ft <sup>3</sup> per Min.		



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

Point No.	$\Theta$ (min)	$V_n$ (ft <sup>3</sup> ) $V_1 =$	$\Delta P$ ("H <sub>2</sub> O)	$(\Delta P)^{1/2}$	$\Delta H$ ("H <sub>2</sub> O)	$T_a$ (°F) $t_1$ $t_2$	$T_s$ (°F)	Vacuum ("Hg)	Final Imp. Temp. (°F)	Filter Temp. (°F)	Remark $K_p = \frac{760}{P_{atm}}$
		797.956									4.19 4.21
51	5	801.73	0.36	0.606	1.53	94 95	84	1.5	62	-	4.25
62	16	804.91	0.37	0.608	1.57	97 95	84	1.5	51	-	4.25
43	15	808.40	0.37	0.608	1.57	99 94	84	1.5	49	-	4.25
204	20	811.73	0.31	0.557	1.32	100 94	84	1.5	48	-	4.25
255	25	814.90	0.32	0.566	1.36	100 94	84	1.5	48	-	4.25
6	30	818.03	0.29	0.534	1.23	101 94	84	1.5	50	-	4.25
7	35	821.10	0.28	0.529	1.19	101 95	84	1.5	49	-	4.25
8	40	823.99	0.25	0.500	1.06	102 95	83	1.0	50	-	4.25
9	45	827.35	0.27	0.520	1.15	102 95	83	1.0	48	-	4.25
10	50	830.52	0.34	0.583	1.44	103 95	83	1.5	49	-	4.25
11	55	833.69	0.36	0.600	1.53	103 95	83	1.5	49	-	4.25
12	60	837.00	0.34	0.583	1.44	103 95	83	1.5	48	-	4.25
13	65	840.57	0.39	0.624	1.66	98 95	83	1.5	54	-	4.25
14	70	844.12	0.39	0.624	1.66	99 95	84	1.5	50	-	4.25
15	75	847.77	0.40	0.632	1.70	103 95	83	2.0	50	-	4.25
16	80	851.13	0.31	0.557	1.32	103 95	83	2.5	50	-	4.25
17	85	854.18	0.32	0.566	1.36	103 96	83	1.5	51	-	4.25
18	90	857.38	0.32	0.566	1.36	103 95	83	1.5	49	-	4.25
19	95	860.57	0.29	0.534	1.23	103 96	83	1.5	47	-	4.25
20	100	863.68	0.27	0.520	1.15	102 96	83	1.0	49	-	4.25
21	105	867.20	0.37	0.608	1.57	103 96	83	1.5	49	-	4.25
22	110	870.00	0.45	0.671	1.91	103 96	84	2.0	50	-	4.25
23	115	874.98	0.48	0.693	2.14	104 96	84	2.0	50	-	4.25
24	120	878.75	0.46	0.678	1.96	104 96	84	2.0	50	-	4.25
TOTAL		80.795	8.71	14.061	36.31	4812	2003 4920				
AVERAGE			6.35	0.586	1.47	100 °F	84 °F				
						560 °R	544 °R				

START 1330 START 1433

STOP 1430 STOP 1537

E-25

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

# ISOKINETIC DATA SHEET<sup>1</sup>

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 5 June 2003

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 7

## FROM FIELD DATA SHEET:

$$C_p = \underline{0.839} \quad T_a = \underline{53.9} \quad A_a = \underline{2876} \quad V_a = \underline{85.137} \quad P_{bar} = \underline{29.37} \quad \sqrt{\Delta P_{avg}} = \underline{0.620}$$

$$\theta = \underline{120} \quad T_m = \underline{55.1} \quad A_m = \underline{3.362 \times 10^{-4}} \quad \gamma_m = \underline{1.009} \quad P_{stat} = \underline{0.24} \quad \Delta H = \underline{1.64}$$

## FROM PHYSICAL SCIENCE:

$$V_{1c} = \underline{31.2} \quad M_a = \underline{\quad} \quad \%CO_2 = \underline{0.0} \quad \%O_2 = \underline{20.9} \quad \%N_2 = \underline{79.1}$$

## PRESSURE CALCULATIONS:

$$P_m = P_{bar} + \frac{\Delta H}{13.6} = ( \quad ) + \frac{( \quad )}{13.6} = \underline{29.46} \text{ in. Hg}$$

$$P_s = P_{bar} + \frac{P_{stat}}{13.6} = ( \quad ) + \frac{( \quad )}{13.6} = \underline{29.35} \text{ in. Hg}$$

## DRY GAS VOLUME:

$$V_{std} = \frac{17.65 V_m \gamma_m P_m}{T_m} = \frac{17.65 ( \quad ) ( \quad ) ( \quad )}{( \quad )} = \underline{81.07} \text{ dscf}$$

## MOISTURE CONTENT:

$$B_{ws} = \frac{V_{wsd}}{V_{msd} + V_{wsd}} = \frac{( \quad )}{( \quad ) + ( \quad )} = \underline{0.018}$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>  
(Continued)

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03, DATE: 5 June 2003

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 7

STACK GAS MOLECULAR WEIGHT:

$$M_s = (1 - B_{wo}) [0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)] + 18B_{wo}$$

$$= (1 - ) [0.44 ( ) + 0.32 ( ) + 0.28 ( )] + 18 ( ) = \underline{28.64} \frac{lb}{lb \text{ mole wet}}$$

STACK GAS VELOCITY:

$$V_{s,avg} = 85.48 C_p \sqrt{\Delta P_{avg}} \sqrt{\frac{T_s}{P_s M_s}} = 85.48 ( ) ( ) \sqrt{\frac{( )}{( ) ( )}} = \underline{35.60} \frac{ft}{sec}$$

STACK GAS VOLUMETRIC FLOW RATE:

$$Q_s = \frac{63,529 (1 - B_{wo}) V_{s,avg} A_s P_s}{T_s} = \frac{63,529 (1 - ) ( ) ( ) ( )}{( )} = \underline{952,843} \frac{dscf}{hr}$$

PERCENT ISOKINETIC:

$$I = \frac{0.0945 T_s V_{s,avg}}{\Theta V_s P_s A_s (1 - B_{wo})} = \frac{0.0945 ( ) ( )}{( ) ( ) ( ) ( ) (1 - )} = \underline{99.1} \%$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

FIELD DATA SHEET		RUN NO. 7		DATE 5 June 2003	
Project Number: 43-EL-5116-03		Installation: Anniston Army Depot, Alabama		Meter Box Operator: S. S. S. S. S.	
Sample Location: Chrome Plating Finishing Complex, BLDG 114					
Type of Sample: Total Chrome Moisture					
Nomograph/Calculator		Nozzle		Pitot Tube	
$\Delta H_s$ 1.86	$\Delta P_{avg}$ 0.36	No.	$D_n$	No.	$C_p$
%H <sub>2</sub> O 2	$P_s/P_a$ 1.0	N-1	0.249	5-1	0.84
$T_a$ 560	$T_s$ 540	↓	0.248	$F_{blockage}$ 1.411	
"C" Factor	$K_p$ 4.25		0.250	$C_{p, eff}$ 0.84	
Ref $\Delta P$		$D_{n, avg}$ 0.249		$A_n$ $3.382 \times 10^{-4}$	
Meter Box No. 90496		Dry Gas Meter $\gamma_s$ 1.009		$D_s$ 38"	$A_s$ 7.876
Filter			Probe		
Type	Number	Length	Liner	Heat Set	
N/A	N/A	3' EST	Quartz		
Initial Leak Check			Initial Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	$0.0 / 0.0$ in. H <sub>2</sub> O per 15 Sec.			
15"	0.004 ft <sup>3</sup> per 1 Min.	at $6.7 / 6.9$ in. H <sub>2</sub> O			
Final Leak Check			Final Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	$0.0 / 0.0$ in. H <sub>2</sub> O per 15 Sec.			
2"	0.001 ft <sup>3</sup> per 1 Min.	at $7.1 / 6.5$ in. H <sub>2</sub> O			
Gas-Bag System Leak Check			Component Leak Check		
Initial	Final	Vacuum (in Hg.)	Leak Rate		
$P_{bar}$ 29.34	$P_{stat}$ 0.20		ft <sup>3</sup> per Min.		
Start Time 0927	End Time 1131		ft <sup>3</sup> per Min.		



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

Point No.	$\Theta$ (min)	$V_n$ (ft <sup>3</sup> ) $V_i =$	$\Delta P$ ("H <sub>2</sub> O)	$(\Delta P)^{1/2}$	$\Delta H$ ("H <sub>2</sub> O)	$T_n$ (°F) $t_i$ $t_r$	$T_a$ (°F)	Vacuum ("Hg)	Final Imp. Temp. (°F)	Filter Temp. (°F)	Remark $K_p =$
		884.552									4.25
1	5	888.31	0.41	0.640	1.74	83 86	77	2.0	58	-	4.25
2	10	891.86	0.40	0.632	1.70	83 86	77	2.0	49	-	4.25
3	15	895.42	0.41	0.640	1.74	88 86	78	2.0	52	-	4.25
4	20	898.95	0.40	0.632	1.70	88 86	78	2.0	51	-	4.25
5	25	902.65	0.38	0.616	1.62	90 86	77	2.0	53	-	4.25
6	30	906.07	0.39	0.624	1.66	91 87	78	2.0	55	-	4.25
7	35	909.75	0.38	0.616	1.62	93 88	78	2.0	56	-	4.25
8	40	913.10	0.34	0.583	1.45	92 87	78	2.0	56	-	4.25
9	45	916.32	0.32	0.566	1.36	92 87	78	1.5	55	-	4.25
10	50	919.99	0.39	0.624	1.66	92 88	78	2.0	56	-	4.25
11	55	923.41	0.38	0.616	1.62	95 89	79	2.0	57	-	4.25
12	60	926.99	0.37	0.608	1.57	96 89	79	1.5	56	-	4.25
13	65	930.54	0.37	0.608	1.57	93 91	78	1.5	56	-	4.25
14	70	933.99	0.37	0.608	1.57	93 90	78	1.5	54	-	4.25
15	75	937.44	0.36	0.600	1.53	93 90	78	1.5	54	-	4.25
16	80	940.95	0.38	0.616	1.62	93 90	78	2.0	56	-	4.25
17	85	944.30	0.35	0.592	1.49	94 90	79	1.5	56	-	4.25
18	90	947.58	0.34	0.583	1.45	95 90	79	1.5	58	-	4.25
19	95	950.91	0.31	0.557	1.32	94 90	79	1.5	56	-	4.25
20	100	954.43	0.38	0.616	1.62	97 91	81	2.0	56	-	4.25
21	105	958.20	0.47	0.686	2.00	97 91	79	2.0	57	-	4.25
22	110	962.00	0.45	0.671	1.91	97 91	79	2.0	57	-	4.25
23	115	965.79	0.46	0.678	1.96	99 92	80	2.0	57	-	4.25
24	120	969.68	0.46	0.678	1.96	100 92	80	2.0	57	-	4.25
TOTAL		85.157	9.27	14.89	39.44	4361	1885				
AVERAGE			0.39	0.620	1.64	91 °F	79 °F				
						551 °R	539 °R				

START 0927      STOP 1031  
 STOP 1027      STOP 1131

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 5 June 2003

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 8

FROM FIELD DATA SHEET:

$$C_p = 0.819 \quad T_s = 544 \quad A_n = 7.876 \quad V_n = 80.903 \quad P_{bar} = 29.34 \quad \sqrt{\Delta P_{avg}} = 0.597$$

$$\theta = 12.0 \quad T_m = 557 \quad A_n = 13824 \quad \gamma_n = 1.009 \quad P_{stat} = 0.20 \quad \Delta H = 1.52$$

FROM PHYSICAL SCIENCE:

$$V_{lc} = 30.9 \quad M_n = \quad \%CO_2 = 0.6 \quad \%O_2 = 20.9 \quad \%N_2 = 79.1$$

PRESSURE CALCULATIONS:

$$P_m = P_{bar} + \frac{\Delta H}{13.6} = ( ) + \frac{( )}{13.6} = 29.45 \text{ in. Hg}$$

$$P_s = P_{bar} + \frac{P_{stat}}{13.6} = ( ) + \frac{( )}{13.6} = 29.35 \text{ in. Hg}$$

DRY GAS VOLUME:

$$V_{nd} = \frac{17.65 V_m \gamma_m P_m}{T_m} = \frac{17.65 ( ) ( ) ( )}{( )} = 76.18 \text{ dscf}$$

MOISTURE CONTENT:

$$B_{wo} = \frac{V_{w,nd}}{V_{m,nd} + V_{w,nd}} = \frac{( )}{( ) + ( )} = 0.019$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

FIELD DATA SHEET		RUN NO. 8		DATE 5 June 2003	
Project Number: 43-EL-5116-03		Installation: Anniston Army Depot, Alabama		Meter Box Operator: S. Monahan, et al.	
Sample Location: Chrome Plating Finishing Complex, BLDG 114					
Type of Sample: Total Chrome Moisture					
Nomograph/Calculator		Nozzle		Pitot Tube	
$\Delta H_e$ 1.86	$\Delta P_{avg}$ 0.36	No.	$D_n$	No.	$C_p$
%H <sub>2</sub> O 2	$P_s/P_n$ 1.0	N-1	0.249	5-3	0.84
$T_n$ 560	$T_s$ 570	↓	0.248	$F_{blockage}$ 1.411	
"C" Factor	$K_p$ 4.25	↓	0.250	$C_{p,eff}$ 0.84	
Ref $\Delta P$		$D_{n,avg}$ 0.249		$A_n$ 3.382 x 10 <sup>-4</sup>	
Meter Box No. 90496		Dry Gas Meter $\gamma_n$ 1.009		$D_s$ 38"	$A_s$ 7.876
Filter			Probe		
Type	Number	Length	Liner	Heat Set	
N/A	N/A	3' Eff	Quartz	—	
Initial Leak Check			Initial Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
15"	0.008 ft <sup>3</sup> per 1 Min.	at 6.1 / 7.3 in. H <sub>2</sub> O			
Final Leak Check			Final Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
2.0"	0.006 ft <sup>3</sup> per 1 Min.	at 7.1 / 16.8 in. H <sub>2</sub> O			
Gas Bag System Leak Check			Component Leak Check		
Initial	Final	Vacuum (in Hg.)	Leak Rate		
$P_{bar}$ 29.34	$P_{stat}$ 0.20		ft <sup>3</sup> per Min.		
Start Time 1155	End Time 1400		ft <sup>3</sup> per Min.		



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

Point No.	Q (min)	V <sub>n</sub> (ft <sup>3</sup> ) V <sub>i</sub> =	ΔP ("H <sub>2</sub> O)	(ΔP) <sup>1/2</sup>	ΔH ("H <sub>2</sub> O)	T <sub>a</sub> (°F) t <sub>i</sub> t <sub>e</sub>	T <sub>s</sub> (°F)	Vacuum ("Hg)	Final Imp. Temp. (°F)	Filter Temp. (°F)	Remark K <sub>p</sub> =
		969.869									4.25
1	5	973.72	0.36	0.600	1.53	93 93	80	2.0	62	-	4.25
2	10	977.69	0.37	0.608	1.57	94 93	81	2.0	60	-	4.25
3	15	980.35	0.38	0.616	1.62	97 93	81	2.0	53	-	4.25
4	20	983.75	0.38	0.616	1.62	99 93	82	2.0	52	-	4.25
5	25	987.29	0.37	0.608	1.57	101 94	83	2.0	51	-	4.25
6	30	990.87	0.29	0.539	1.23	101 94	83	2.0	52	-	4.25
7	35	993.35	0.30	0.548	1.28	100 94	84	2.0	52	-	4.25
8	40	996.39	0.26	0.510	1.11	100 93	84	2.0	50	-	4.25
9	45	999.28	0.25	0.500	1.06	100 94	84	1.5	49	-	4.25
10	50	1002.27	0.29	0.534	1.23	100 94	85	1.5	49	-	4.25
11	55	1005.07	0.29	0.534	1.23	100 94	85	1.5	50	-	4.25
12	60	1007.786	0.28	0.529	1.19	101 94	85	1.5	51	-	4.25
13	65	1011.59	0.43	0.656	1.83	96 94	84	2.0	55	-	4.25
14	70	1015.27	0.42	0.648	1.79	97 94	84	2.0	53	-	4.25
15	75	1019.00	0.43	0.656	1.83	99 93	85	2.0	51	-	4.25
16	80	1022.74	0.43	0.656	1.83	102 93	85	2.0	51	-	4.25
17	85	1026.36	0.42	0.648	1.79	102 94	85	2.0	48	-	4.25
18	90	1029.87	0.38	0.616	1.62	103 94	85	2.0	49	-	4.25
19	95	1032.90	0.26	0.510	1.11	104 94	85	2.0	49	-	4.25
20	100	1038.07	0.29	0.539	1.23	101 94	86	1.5	49	-	4.25
21	105	1039.53	0.37	0.608	1.57	101 94	84	2.0	48	-	4.25
22	110	1043.14	0.41	0.640	1.74	103 95	84	2.0	49	-	4.25
23	115	1046.95	0.46	0.678	2.00	102 94	84	2.0	48	-	4.25
24	120	1050.772	0.45	0.671	1.91	101 94	84	2.0	49	-	4.25
TOTAL		80.903	8.57	14.328	36.49	4647	2012				
AVERAGE			0.36	0.597	1.52	97 °F	84 °F				
						557 °R	544 °R				

START 1155

START 1300

STOP 1255

STOP 1400

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

FIELD DATA SHEET		RUN NO. 8		DATE 5 June 2003	
Project Number: 43-EL-5116-03		Installation: Anniston Army Depot, Alabama		Meter Box Operator: S. H. H. H.	
Sample Location: Chrome Plating Finishing Complex, BLDG 114					
Type of Sample: Total Chrome Moisture					
Nomograph/Calculator		Nozzle		Pitot Tube	
$\Delta H_g$ 1.86	$\Delta P_{avg}$ 0.36	No.	$D_n$	No.	$C_p$
%H <sub>2</sub> O 2	$P_a/P_m$ 1.0	N-1	0.249	5-3	0.84
$T_m$ 560	$T_a$ 570		0.248	$E_{blockage}$ 1.411	
"C" Factor	$K_p$ 4.25		0.250	$C_{p,eff}$ 0.84	
Ref $\Delta P$		$D_{n,avg}$ 0.249		$A_n$ 3.382 x 10 <sup>-4</sup>	
Meter Box No. 90496		Dry Gas Meter $\gamma_m$ 1.009		$D_s$ 38"	$A_s$ 7.876
Filter			Probe		
Type	Number	Length	Liner	Heat Set	
N/A	N/A	3' Eff	Quartz	—	
Initial Leak Check			Initial Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
15"	0.008 ft <sup>3</sup> per 1 Min.	at 6.1 / 7.3 in. H <sub>2</sub> O			
Final Leak Check			Final Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
2.0"	0.006 ft <sup>3</sup> per 1 Min.	at 7.1 / 8.8 in. H <sub>2</sub> O			
Gas Bag System Leak Check			Component Leak Check		
Initial	Final	Vacuum (in Hg.)	Leak Rate		
$P_{bar}$ 29.54	$P_{stat}$ 0.20		ft <sup>3</sup> per Min.		
Start Time 1155	End Time 1406		ft <sup>3</sup> per Min.		

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

# ISOKINETIC DATA SHEET<sup>1</sup>

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 6/5/03

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 9

## FROM FIELD DATA SHEET:

$$C_p = 0.839 \quad T_s = 546 \quad A_o = 7.676 \quad V_a = 81.731 \quad P_{bar} = 29.39 \quad \sqrt{\Delta P_{avg}} = 0.591$$

$$\theta = 12.0 \quad T_m = 561 \quad A_n = 3.3824 \quad \gamma_n = 1.009 \quad P_{stat} = 0.26 \quad \Delta H = 1.50$$

## FROM PHYSICAL SCIENCE:

$$V_{lc} = 29.2 \quad M_n = \quad \%CO_2 = 0.0 \quad \%O_2 = 20.9 \quad \%N_2 = 79.1$$

## PRESSURE CALCULATIONS:

$$P_m = P_{bar} + \frac{\Delta H}{13.6} = ( ) + \frac{( )}{13.6} = 29.45 \text{ in. Hg}$$

$$P_s = P_{bar} + \frac{P_{stat}}{13.6} = ( ) + \frac{( )}{13.6} = 29.35 \text{ in. Hg}$$

## DRY GAS VOLUME:

$$V_{md} = \frac{17.65 V_m \gamma_m P_m}{T_m} = \frac{17.65 ( ) ( ) ( )}{( )} = 76.50 \text{ dscf}$$

## MOISTURE CONTENT:

$$B_{wo} = \frac{V_{wmd}}{V_{md} + V_{wmd}} = \frac{( )}{( ) + ( )} = 0.018$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

ISOKINETIC DATA SHEET<sup>1</sup>  
(Continued)

INSTALLATION: Anniston Army Depot, AL PROJECT NUMBER: 43-EL-5116-03 DATE: 6/5/03

LOCATION: Chrome Plating Finishing Complex, BLDG 114

RUN NUMBER: 9

STACK GAS MOLECULAR WEIGHT:

$$M_s = (1 - B_{wo}) [0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)] + 18B_{wo}$$

$$= (1 - ) [0.44 ( ) + 0.32 ( ) + 0.28 ( )] + 18 ( ) = \underline{28.64} \frac{lb}{lb \text{ mole wet}}$$

STACK GAS VELOCITY:

$$V_{s,avg} = 85.48 C_p \sqrt{\Delta P_{avg}} \sqrt{\frac{T_s}{P_s M_s}} = 85.48 ( ) ( ) \sqrt{\frac{( )}{( ) ( )}} = \underline{34.15} \frac{ft}{sec}$$

STACK GAS VOLUMETRIC FLOW RATE:

$$Q_s = \frac{63,529 (1 - B_{wo}) V_{s,avg} A_s P_s}{T_s} = \frac{63,529 (1 - ) ( ) ( ) ( )}{( )} = \underline{902,542} \frac{dscf}{hr}$$

PERCENT ISOKINETIC:

$$I = \frac{0.0945 T_s V_{s,avg}}{\Theta V_s P_s A_n (1 - B_{wo})} = \frac{0.0945 ( ) ( )}{( ) ( ) ( ) ( ) (1 - )} = \underline{98.8} \%$$

<sup>1</sup> Standard Temperature = 68°F (528°R); Standard Pressure = 29.92 in. Hg

## Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

FIELD DATA SHEET		RUN NO. 9		DATE 5 June 2003	
Project Number: 43-EL-5116-03		Installation: Anniston Army Depot, Alabama		Meter Box Operator: S. H. H. H. H.	
Sample Location: Chrome Plating Finishing Complex, BLDG 114					
Type of Sample: <u>Total Chrome</u> <u>Moisture</u>					
Nomograph/Calculator		Nozzle		Pitot Tube	
$\Delta H_s$ 1.86	$\Delta P_{avg}$ 0.36	No.	$D_n$	No.	$C_p$
%H <sub>2</sub> O 2	$P_s/P_n$ 1.0	N-1	0.249	5-3	0.84
$T_n$ 560	$T_s$ 540	↓	0.248	$F_{blockage}$ 1.411	
"C" Factor	$K_p$ 4.25	↓	0.250	$C_{p,corr}$ 0.84	
Ref $\Delta P$		$D_{n,avg}$ 0.249		$A_n$ $3.382 \times 10^{-4}$	
Meter Box No. 90496		Dry Gas Meter $\gamma_m$ 1.009		$D_s$ 38"	$A_s$ 7.876
Filter			Probe		
Type	Number	Length	Liner	Heat Set	
N/A	N/A	3' E88	Quartz		
Initial Leak Check			Initial Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	0.0 / 0.0 in. H <sub>2</sub> O per 15 Sec.			
15"	0.001 ft <sup>3</sup> per / Min.	at 6.4 / 6.8 in. H <sub>2</sub> O			
Final Leak Check			Final Pitot Tube Leak Check		
Vacuum (in. Hg)	Leak Rate	/ in. H <sub>2</sub> O per 15 Sec.			
25"	0.001 ft <sup>3</sup> per / Min.	at / in. H <sub>2</sub> O			
Gas Bag System Leak Check			Component Leak Check		
Initial	Final	Vacuum (in. Hg.)	Leak Rate		
$P_{bar}$ 29.34	$P_{stat}$ 0.20		ft <sup>3</sup> per Min.		
Start Time 1425	End Time 1625		ft <sup>3</sup> per Min.		

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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

MOISTURE DATA SHEETS

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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## LAB DATA SHEET

PART I - GENERAL:

INSTALLATION: Anniston Army Depot

ANALYST: Louis M. McCarter

SOURCE: Chrome Electroplating Facility

BAROMETRIC PRESSURE(In, Hg): 29.13SAMPLING DATE: 6/3/03

SAMPLING SITE: LEVEL

TIME OF SAMPLING: 1115RUN #: AAD - 1TRAIN: RM 306PART II - MOISTURE DETERMINATION

IMPINGER #	1	2	3	4
CONTENTS	100 ml. 0.1 N NaOH	100 ml. 0.1 N NaOH	DRY	Silica Gel
FINAL WEIGHT (g.):	<u>718.6</u>	<u>601.8</u>	<u>593.8</u>	<u>842.6</u>
INITIAL WEIGHT (g.):	<u>700.1</u>	<u>593.0</u>	<u>591.2</u>	<u>826.2</u>
DIFFERENCE (g.):	<u>18.5</u>	<u>8.8</u>	<u>2.6</u>	<u>16.4</u>
TOTAL MOISTURE (g.) =				<u>46.3</u>

PART III - VOLUME OF FIRST THREE IMPINGERS.

TOTAL FINAL VOLUME: \_\_\_\_\_ ml.

TOTAL INITIAL VOLUME: 200 ml.

DIFFERENCE: \_\_\_\_\_ ml.

beginning pH = 11.0

Final pH = 10.5

~~Impingers~~PART IV - TOTAL VOLUME OF SAMPLE CONTAINER.TOTAL FINAL VOLUME OF IMPINGERS,  
PROBE RINSE AND CONNECTING GLASSWARE RINSE :~~525~~ ml.AUTHENTICATION:TECHNICIAN: for M. M. CarterPROJECT OFFICER: E. D. Y. N.

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## LAB DATA SHEET

PART I - GENERAL:

INSTALLATION : Anniston Army Depot

ANALYST : Louis M. McCarter

SOURCE : Chrome Electroplating Facility

BAROMETRIC PRESSURE(In, Hg) : 29.13SAMPLING DATE : 6/3/03

SAMPLING SITE : LEVEL

TIME OF SAMPLING : 1425RUN # : AAD - 2TRAIN : RM 306PART II - MOISTURE DETERMINATION

IMPINGER #	1	2	3	4
	100 ml. 0.1 N NaOH	100 ml. 0.1 N NaOH	DRY	Silica Gel
CONTENTS				
FINAL WEIGHT (g.) :	<u>744.9</u>	<u>676.7</u>	<u>598.6</u>	<u>765.2</u>
INITIAL WEIGHT (g.) :	<u>721.9</u>	<u>669.9</u>	<u>595.9</u>	<u>749.6</u>
DIFFERENCE (g.) :	<u>23.0</u>	<u>6.8</u>	<u>2.7</u>	<u>15.6</u>
TOTAL MOISTURE (g.) =				<u>48.1</u>

PART III - VOLUME OF FIRST THREE IMPINGERS.

TOTAL FINAL VOLUME : \_\_\_\_\_ ml.

TOTAL INITIAL VOLUME : 200 ml.

DIFFERENCE : \_\_\_\_\_ ml.

begin pH = 11.0  
Final pH = 10.5

PART IV - TOTAL VOLUME OF SAMPLE CONTAINER.TOTAL FINAL VOLUME OF IMPINGERS,  
PROBE RINSE AND CONNECTING GLASSWARE RINSE :450 ml.AUTHENTICATION :TECHNICIAN : for M. McCarterPROJECT OFFICER : Ed D. [Signature]



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

LAB DATA SHEET

PART I - GENERAL:

INSTALLATION: Anniston Army Depot

ANALYST: Louis M. McCarter

SOURCE: Chrome Electroplating Facility

BAROMETRIC PRESSURE (In. Hg): 29.13

SAMPLING DATE: 6/3/03

SAMPLING SITE: LEVEL

TIME OF SAMPLING: 1700

RUN #: AAD - 3

TRAIN: RM 306

PART II - MOISTURE DETERMINATION

IMPINGER #	1	2	3	4
CONTENTS	100 ml. 0.1 N NaOH	100 ml. 0.1 N NaOH	DRY	Silica Gel
FINAL WEIGHT (g.): →	<u>723.8</u>	<u>674.5</u>	<u>590.9</u>	<u>731.1</u>
INITIAL WEIGHT (g.):	<u>696.9</u>	<u>670.1</u>	<u>588.8</u>	<u>716.8</u>
DIFFERENCE (g.):	<u>26.9</u>	<u>4.4</u>	<u>2.1</u>	<u>14.3</u>
TOTAL MOISTURE (g.) =				<u>47.7</u>

PART III - VOLUME OF FIRST THREE IMPINGERS.

TOTAL FINAL VOLUME: \_\_\_\_\_ ml.  
TOTAL INITIAL VOLUME: 200 ml.  
DIFFERENCE: \_\_\_\_\_ ml.

begin pH = 11.0

Final pH = 10.0

~~10.0~~

~~10.0~~

PART IV - TOTAL VOLUME OF SAMPLE CONTAINER.

TOTAL FINAL VOLUME OF IMPINGERS,  
PROBE RINSE AND CONNECTING GLASSWARE RINSE:

450 ml.

AUTHENTICATION:

TECHNICIAN: Jon M. McCarter

PROJECT OFFICER: T. J. D. J.

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## LAB DATA SHEET

PART I - GENERAL:

INSTALLATION : Anniston Army Depot

ANALYST : Louis M. McCarter

SOURCE : Chrome Electroplating Facility

BAROMETRIC PRESSURE(In, Hg) : 29.19SAMPLING DATE : 6/4/03

SAMPLING SITE : LEVEL

TIME OF SAMPLING : 0820RUN # : AAD - 4TRAIN : RM 306PART II - MOISTURE DETERMINATION

IMPINGER #	1	2	3	4
	100 ml. 0.1 N NaOH	100 ml. 0.1 N NaOH	DRY	Silica Gel
FINAL WEIGHT (g.) :	<u>731.0</u>	<u>692.7</u>	<u>620.5</u>	<u>803.0</u>
INITIAL WEIGHT (g.) :	<u>718.8</u>	<u>688.9</u>	<u>618.9</u>	<u>788.0</u>
DIFFERENCE (g.) :	<u>12.2</u>	<u>3.8</u>	<u>1.6</u>	<u>15</u>
TOTAL MOISTURE (g.) =				<u>32.6</u>

PART III - VOLUME OF FIRST THREE IMPINGERS.

TOTAL FINAL VOLUME : \_\_\_\_\_ ml.

TOTAL INITIAL VOLUME : 200 ml.

DIFFERENCE : \_\_\_\_\_ ml.

Beginning pH = 9.5

Final pH = 8.5

PART IV - TOTAL VOLUME OF SAMPLE CONTAINER.TOTAL FINAL VOLUME OF IMPINGERS,  
PROBE RINSE AND CONNECTING GLASSWARE RINSE :450 ml.AUTHENTICATION :

TECHNICIAN :

Louis M. McCarter

PROJECT OFFICER :

Jeff D. Yea

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## LAB DATA SHEET

PART I - GENERAL:

INSTALLATION : Anniston Army Depot

ANALYST : Louis M. McCarter

SOURCE : Chrome Electroplating Facility

BAROMETRIC PRESSURE(In, Hg) : 29.19SAMPLING DATE : 6/4/03

SAMPLING SITE : LEVEL

TIME OF SAMPLING : 1100RUN # : AAD - 5TRAIN : RM 306PART II - MOISTURE DETERMINATION

IMPINGER #	1	2	3	4
	100 ml. 0.1 N NaOH	100 ml. 0.1 N NaOH	DRY	Silica Gel
CONTENTS				
FINAL WEIGHT (g.):	<u>734.7</u>	<u>673.9</u>	<u>620.5</u>	<u>747.3</u>
INITIAL WEIGHT (g.):	<u>719.0</u>	<u>670.2</u>	<u>618.9</u>	<u>734.0</u>
DIFFERENCE (g.):	<u>15.7</u>	<u>3.7</u>	<u>1.6</u>	<u>13.3</u>
TOTAL MOISTURE (g.) =				<u>34.3</u>

PART III - VOLUME OF FIRST THREE IMPINGERS:

TOTAL FINAL VOLUME : \_\_\_\_\_ ml.

TOTAL INITIAL VOLUME : 200 ml.

DIFFERENCE : \_\_\_\_\_ ml.

Beginning pH = 9.5

Final pH = 8.5

PART IV - TOTAL VOLUME OF SAMPLE CONTAINER.

TOTAL FINAL VOLUME OF IMPINGERS,

PROBE RINSE AND CONNECTING GLASSWARE RINSE : 450 ml.AUTHENTICATION :TECHNICIAN : for M. McCarterPROJECT OFFICER : CF D JH

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## LAB DATA SHEET

PART I - GENERAL:

INSTALLATION: Anniston Army Depot

ANALYST: Louis M. McCarter

SOURCE: Chrome Electroplating Facility

BAROMETRIC PRESSURE(In, Hg): 29.19SAMPLING DATE: 6/4/03

SAMPLING SITE: LEVEL

TIME OF SAMPLING: 1330RUN #: AAD-6TRAIN: RM 306PART II - MOISTURE DETERMINATION

IMPINGER #	1	2	3	4
CONTENTS	100 ml. 0.1 N NaOH	100 ml. 0.1 N NaOH	DRY	Silica Gel
FINAL WEIGHT (g.):	<u>746.5</u>	<u>667.7</u>	<u>616.4</u>	<u>724.8</u>
INITIAL WEIGHT (g.):	<u>730.5</u>	<u>663.8</u>	<u>614.9</u>	<u>711.7</u>
DIFFERENCE (g.):	<u>16.0</u>	<u>3.9</u>	<u>1.5</u>	<u>13.1</u>
TOTAL MOISTURE (g.) =				<u>34.5</u>

PART III - VOLUME OF FIRST THREE IMPINGERS.

TOTAL FINAL VOLUME: \_\_\_\_\_ ml.

TOTAL INITIAL VOLUME: 200 ml.

DIFFERENCE: \_\_\_\_\_ ml.

Begin pH = 9.5

Final pH = 8.5

PART IV - TOTAL VOLUME OF SAMPLE CONTAINER.

TOTAL FINAL VOLUME OF IMPINGERS,

PROBE RINSE AND CONNECTING GLASSWARE RINSE:

450 ml.AUTHENTICATION:

TECHNICIAN:

for M. McCarter

PROJECT OFFICER:

CFD

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## LAB DATA SHEET

PART I - GENERAL:

INSTALLATION : Anniston Army Depot

ANALYST : Louis M. McCarter

SOURCE : Chrome Electroplating Facility

BAROMETRIC PRESSURE(In, Hg) : 29.34SAMPLING DATE : 6/5/03

SAMPLING SITE : LEVEL

TIME OF SAMPLING : 0927RUN # : AAD - 2TRAIN : RM 306PART II - MOISTURE DETERMINATION

IMPINGER #	1	2	3	4
	100 ml. 0.1 N NaOH	100 ml. 0.1 N NaOH	DRY	Silica Gel
FINAL WEIGHT (g.):	<u>747.0</u>	<u>727.0</u>	<u>630.8</u>	<u>778.3</u>
INITIAL WEIGHT (g.):	<u>739.0</u> <u>736.9</u>	<u>722.4</u> <u>718.5</u>	<u>628.6</u>	<u>761.9</u>
DIFFERENCE (g.):	<u>8.0</u>	<u>4.6</u>	<u>2.2</u>	<u>16.4</u>
TOTAL MOISTURE (g.) =				<u>31.2</u>

PART III - VOLUME OF FIRST THREE IMPINGERS.

TOTAL FINAL VOLUME : \_\_\_\_\_ ml.

TOTAL INITIAL VOLUME : 200 ml.

DIFFERENCE : \_\_\_\_\_ ml.

Beginning pH = 13.0

Final pH = 12.0

PART IV - TOTAL VOLUME OF SAMPLE CONTAINER.TOTAL FINAL VOLUME OF IMPINGERS,  
PROBE RINSE AND CONNECTING GLASSWARE RINSE :450 ml.AUTHENTICATION :TECHNICIAN : for M. McCarterPROJECT OFFICER : T. J. O. G.



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## LAB DATA SHEET

PART I - GENERAL:

INSTALLATION : Anniston Army Depot

ANALYST : Louis M. McCarter

SOURCE : Chrome Electroplating Facility

BAROMETRIC PRESSURE(In, Hg) : 29.34SAMPLING DATE : 6/5/03

SAMPLING SITE : LEVEL

TIME OF SAMPLING : 1155RUN # : AAD - 8TRAIN : RM 306PART II - MOISTURE DETERMINATION

IMPINGER #	1	2	3	4
CONTENTS	100 ml. 0.1 N NaOH	100 ml. 0.1 N NaOH	DRY	Silica Gel
FINAL WEIGHT (g.) :	<u>749.0</u>	<u>722.3</u>	<u>638.3</u>	<u>751.3</u>
INITIAL WEIGHT (g.) :	<u>238.8</u>	<u>717.6</u>	<u>636.7</u>	<u>736.9</u>
DIFFERENCE (g.) :	<u>10.2</u>	<u>4.7</u>	<u>1.6</u>	<u>14.4</u>
TOTAL MOISTURE (g.) =				<u>30.9</u>

PART III - VOLUME OF FIRST THREE IMPINGERS.

TOTAL FINAL VOLUME : \_\_\_\_\_ ml.

TOTAL INITIAL VOLUME : 200 ml.

DIFFERENCE : \_\_\_\_\_ ml.

Beginning pH = 13.0

Final pH = 12.5

PART IV - TOTAL VOLUME OF SAMPLE CONTAINER.

TOTAL FINAL VOLUME OF IMPINGERS,

PROBE RINSE AND CONNECTING GLASSWARE RINSE : 450 ml.AUTHENTICATION :

TECHNICIAN :

for M. N. Cade

PROJECT OFFICER :

E. P. D. J.

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## LAB DATA SHEET

PART I - GENERAL:

INSTALLATION: Anniston Army Depot

ANALYST: Louis M. McCarter

SOURCE: Chrome Electroplating Facility

BAROMETRIC PRESSURE (In, Hg): 29.34SAMPLING DATE: 6/5/03

SAMPLING SITE: LEVEL

TIME OF SAMPLING: 1423RUN #: AAD-9TRAIN: RM 306PART II - MOISTURE DETERMINATION

IMPINGER #	1	2	3	4
	100 ml. 0.1 N NaOH	100 ml. 0.1 N NaOH	DRY	Silica Gel
CONTENTS				
FINAL WEIGHT (g.):	<u>743.7</u>	<u>727.0</u>	<u>637.3</u>	<u>731.3</u>
INITIAL WEIGHT (g.):	<u>734.1</u>	<u>723.1</u>	<u>635.5</u>	<u>717.4</u>
DIFFERENCE (g.):	<u>9.6</u>	<u>3.9</u>	<u>1.8</u>	<u>13.9</u>
TOTAL MOISTURE (g.) =				<u>29.2</u>

PART III - VOLUME OF FIRST THREE IMPINGERS.

TOTAL FINAL VOLUME: \_\_\_\_\_ ml.

TOTAL INITIAL VOLUME: 200 ml.

DIFFERENCE: \_\_\_\_\_ ml.

Begin pH = 13.0

Final pH = 12.5

PART IV - TOTAL VOLUME OF SAMPLE CONTAINER.TOTAL FINAL VOLUME OF IMPINGERS,  
PROBE RINSE AND CONNECTING GLASSWARE RINSE:450 ml.AUTHENTICATION:TECHNICIAN: for M. McCarterPROJECT OFFICER: CFD GH

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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

APPENDIX G

TSP SAMPLER DATA SUMMARY

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Air Pollution Management Study No. 43-EL-5116-03, 3-

TSP SAMPLER WEST FIELD DATA SHEET

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## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-03-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	WEST 1
<b>Operator:</b>	Sutphin	<b>Filter ID No.</b>	Q0113427
<b>Pa (mm Hg)</b>	740.41	<b>Sampler S/N:</b>	0510
<b>Ta (°K)</b>	297.9	<b>Start Time:</b>	1112
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1312

## Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	5.8
Final Pex (in. H <sub>2</sub> O)	5.6
Mean Pex (in. H <sub>2</sub> O)	5.7

## Sampler:

## Regression Values

m=	1.4679
b=	0.0166
r=	0.9999

**Comments:** Elapsed Time; Start: 00202.80 End: 00204.79

Check Point @ 1207 hrs, 5.7 in H<sub>2</sub>O

## Total Time:

Minutes  Mean Qa (m<sup>3</sup>/min)=

## Laboratory Calculations:

Mean Qstd (m<sup>3</sup>/min)=

Vstd (m<sup>3</sup>)=

TSP Concentration =

## Filter Weights (grams):

Final (Wf)

Initial (Wi)

Net (Wn)

## Formulas and Definitions

Mean Qstd = [(Delta Pex)(Pa/760)(298/Ta)]<sup>1/2</sup> -b)(1/m)

Mean Qa = Mean Qstd(760/Pa)(Ta/298)

Vstd = (Qstd)\*(Total Time)

TSP Concentration (micrograms/m<sup>3</sup>) = (Wn)(10<sup>6</sup>)/Vstd

Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates

Pav & Tav = Daily Mean Baro. Pressure and Temperature

Mean Qa range must be 1.1 to 1.7 m<sup>3</sup>/min.



## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-03-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	WEST 2
<b>Operator:</b>	Sutphin	<b>Filter ID No.</b>	Q0113425
<b>Pa (mm Hg)</b>	740.16	<b>Sampler S/N:</b>	0510
<b>Ta (°K)</b>	297.7	<b>Start Time:</b>	1422
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1622

**Sampler Motor Manometer Readings:**

Initial Pex (in. H <sub>2</sub> O)	5.6
Final Pex (in. H <sub>2</sub> O)	5.5
Mean Pex (in. H <sub>2</sub> O)	5.6

**Sampler:****Regression Values**

m=	1.4679
b=	0.0166
r=	0.9999

**Comments:** Elapsed Time; Start: 00204.80 End: 00206.79

Check Point @ 1519 hrs, 5.5 in H<sub>2</sub>O

**Total Time:**

Minutes  Mean Qa (m<sup>3</sup>/min)=

**Laboratory Calculations:****Filter Weights (grams):**

Mean Qstd (m <sup>3</sup> /min)=	<input type="text" value="1.57"/>	Final (Wf)	<input type="text" value="N/A"/>
Vstd (m <sup>3</sup> )=	<input type="text" value="188.80"/>	Initial (Wi)	<input type="text" value="N/A"/>
TSP Concentration =	<input type="text" value="N/A"/>	Net (Wn)	<input type="text" value="N/A"/>

**Formulas and Definitions**

$$\text{Mean Qstd} = [(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})^{1/2} - b](1/m)$$

$$\text{Mean Qa} = \text{Mean Qstd}(760/\text{Pa})(\text{Ta}/298)$$

$$\text{Vstd} = (\text{Qstd})(\text{Total Time})$$

$$\text{TSP Concentration (micrograms/m}^3\text{)} = (\text{Wn})(10^6)/\text{Vstd}$$

$$\text{Mean Qa \& Qstd} = \text{Mean Daily Actual \& Standard Flow Rates}$$

$$\text{Pav \& Tav} = \text{Daily Mean Baro. Pressure and Temperature}$$

Mean Qa range must be 1.1 to 1.7 m<sup>3</sup>/min.

## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-03-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	WEST 3
<b>Operator:</b>	Sutphin	<b>Filter ID No.</b>	Q0113423
<b>Pa (mm Hg)</b>	738.89	<b>Sampler S/N:</b>	0510
<b>Ta (°K)</b>	298	<b>Start Time:</b>	1700
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1900

Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	5.4
Final Pex (in. H <sub>2</sub> O)	5.3
Mean Pex (in. H <sub>2</sub> O)	5.4

Sampler:Regression Values

m=	1.4679
b=	0.0166
r=	0.9999

**Comments:** Elapsed Time; Start: 00206.79 End: 00208.79

Check Point @ 1802 hrs, 5.3 in H<sub>2</sub>O

Total Time:

Minutes  Mean Qa (m3/min)=

Laboratory Calculations:Filter Weights (grams):

Mean Qstd (m3/min)=	<input type="text" value="1.54"/>	Final (Wf)	<input type="text" value="N/A"/>
Vstd (m3)=	<input type="text" value="185.09"/>	Initial (Wi)	<input type="text" value="N/A"/>
TSP Concentration =	<input type="text" value="N/A"/>	Net (Wn)	<input type="text" value="N/A"/>

Formulas and Definitions

$$\text{Mean Qstd} = [(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})^{1/2} - b](1/m)$$

$$\text{Mean Qa} = \text{Mean Qstd}(760/\text{Pa})(\text{Ta}/298)$$

$$\text{Vstd} = (\text{Qstd})(\text{Total Time})$$

$$\text{TSP Concentration (micrograms/m3)} = (\text{Wn})(10^6)/\text{Vstd}$$

Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates

Pav & Tav = Daily Mean Baro. Pressure and Temperature

Mean Qa range must be 1.1 to 1.7 m3/min.

## TSP SAMPLER FIELD DATA SHEET

<u>Installation:</u>	Anniston Army Depot	<u>Date:</u>	06-04-03
<u>Site ID:</u>	Crome Plating Facility	<u>Run Number:</u>	WEST 4
<u>Operator:</u>	Sutphin	<u>Filter ID No.</u>	Q0113421
<u>Pa (mm Hg)</u>	741.43	<u>Sampler S/N:</u>	0510
<u>Ta (°K)</u>	294.5	<u>Start Time:</u>	0825
<u>Equip. Type:</u>	Graseby TSP Sampler	<u>Stop Time:</u>	1025

Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	5.4
Final Pex (in. H <sub>2</sub> O)	5.3
Mean Pex (in. H <sub>2</sub> O)	5.4

Sampler:Regression Values

m=	1.4679
b=	0.0166
r=	0.9999

Comments: Elapsed Time; Start: 00208.79 End: 00210.79

Check Point @ 0926 hrs; 5.3 in H<sub>2</sub>O

Total Time:

Minutes  Mean Qa (m3/min)=

Laboratory Calculations:Filter Weights (grams):

<u>Mean Qstd (m3/min)=</u>	<input type="text" value="1.55"/>	<u>Final (Wf)</u>	<input type="text" value="N/A"/>
<u>Vstd (m3)=</u>	<input type="text" value="186.51"/>	<u>Initial (Wi)</u>	<input type="text" value="N/A"/>
<u>TSP Concentration =</u>	<input type="text" value="N/A"/>	<u>Net (Wn)</u>	<input type="text" value="N/A"/>

Formulas and Definitions

$$\text{Mean Qstd} = [(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})^{1/2} - b](1/m)$$

$$\text{Mean Qa} = \text{Mean Qstd}(760/\text{Pa})(\text{Ta}/298)$$

$$\text{Vstd} = (\text{Qstd})(\text{Total Time})$$

$$\text{TSP Concentration (micrograms/m3)} = (\text{Wn})(10^6)/\text{Vstd}$$

Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates

Pav & Tav = Daily Mean Baro. Pressure and Temperature

Mean Qa range must be 1.1 to 1.7 m3/min.



## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-03-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	WEST 3
<b>Operator:</b>	Sutphin	<b>Filter ID No.</b>	Q0113423
<b>Pa (mm Hg)</b>	738.89	<b>Sampler S/N:</b>	0510
<b>Ta (°K)</b>	298	<b>Start Time:</b>	1700
<b>Equip.Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1900

**Sampler Motor Manometer Readings:**

Initial Pex (in. H <sub>2</sub> O)	5.4
Final Pex (in. H <sub>2</sub> O)	5.3
Mean Pex (in. H <sub>2</sub> O)	5.4

**Sampler:****Regression Values**

m=	1.4679
b=	0.0166
r=	0.9999

**Comments:** Elapsed Time; Start: 00206.79 End: 00208.79

Check Point @ 1802 hrs, 5.3 in H<sub>2</sub>O

**Total Time:**

Minutes  Mean Qa (m<sup>3</sup>/min)=

**Laboratory Calculations:****Filter Weights (grams):**

Mean Qstd (m <sup>3</sup> /min)=	<input type="text" value="1.54"/>	Final (Wf)	<input type="text" value="N/A"/>
Vstd (m <sup>3</sup> )=	<input type="text" value="185.09"/>	Initial (Wi)	<input type="text" value="N/A"/>
TSP Concentration =	<input type="text" value="N/A"/>	Net (Wn)	<input type="text" value="N/A"/>

**Formulas and Definitions**

$$\text{Mean Qstd} = [(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})^{1/2} - b](1/m)$$

$$\text{Mean Qa} = \text{Mean Qstd}(760/\text{Pa})(\text{Ta}/298)$$

$$\text{Vstd} = (\text{Qstd})(\text{Total Time})$$

$$\text{TSP Concentration (micrograms/m}^3\text{)} = (\text{Wn})(10^6)/\text{Vstd}$$

Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates

Pav & Tav = Daily Mean Baro. Pressure and Temperature

Mean Qa range must be 1.1 to 1.7 m<sup>3</sup>/min.

## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-04-03
<b>Site ID:</b>	Chrome Plating Facility	<b>Run Number:</b>	WEST 4
<b>Operator:</b>	Sutphin	<b>Filter ID No.:</b>	Q0113421
<b>Pa (mm Hg)</b>	741.43	<b>Sampler S/N:</b>	0510
<b>Ta (°K)</b>	294.5	<b>Start Time:</b>	0825
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1025

## Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	5.4
Final Pex (in. H <sub>2</sub> O)	5.3
Mean Pex (in. H <sub>2</sub> O)	5.4

## Sampler:

## Regression Values

m=	1.4679
b=	0.0166
r=	0.9999

**Comments:** Elapsed Time; Start: 00208.79 End: 00210.79

Check Point @ 0926 hrs, 5.3 in H<sub>2</sub>O

## Total Time:

Minutes  Mean Qa (m<sup>3</sup>/min)=

## Laboratory Calculations:

## Filter Weights (grams):

Mean Qstd (m <sup>3</sup> /min)=	<input type="text" value="1.55"/>	Final (Wf)	<input type="text" value="N/A"/>
Vstd (m <sup>3</sup> )=	<input type="text" value="186.51"/>	Initial (Wi)	<input type="text" value="N/A"/>
TSP Concentration =	<input type="text" value="N/A"/>	Net (Wn)	<input type="text" value="N/A"/>

## Formulas and Definitions

$$\text{Mean Qstd} = [(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})^{1/2} - b](1/m)$$

$$\text{Mean Qa} = \text{Mean Qstd}(760/\text{Pa})(\text{Ta}/298)$$

$$\text{Vstd} = (\text{Qstd})(\text{Total Time})$$

$$\text{TSP Concentration (micrograms/m}^3\text{)} = (\text{Wn})(10^6)/\text{Vstd}$$

$$\text{Mean Qa \& Qstd} = \text{Mean Daily Actual \& Standard Flow Rates}$$

$$\text{Pav \& Tav} = \text{Daily Mean Baro. Pressure and Temperature}$$

$$\text{Mean Qa range must be 1.1 to 1.7 m}^3\text{/min.}$$



## TSP SAMPLER FIELD DATA SHEET

<u>Installation:</u>	Anniston Army Depot	<u>Date:</u>	06-04-03
<u>Site ID:</u>	Crome Plating Facility	<u>Run Number:</u>	WEST 5
<u>Operator:</u>	Sutphin	<u>Filter ID No.:</u>	Q0113419
<u>Pa (mm Hg)</u>	741.43	<u>Sampler S/N:</u>	0510
<u>Ta (°K)</u>	294.5	<u>Start Time:</u>	1105
<u>Equip. Type:</u>	Graseby TSP Sampler	<u>Stop Time:</u>	1305

Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	5.3
Final Pex (in. H <sub>2</sub> O)	5.2
Mean Pex (in. H <sub>2</sub> O)	5.3

Sampler:Regression Values

m=	1.4679
b=	0.0166
r=	0.9999

Comments: Elapsed Time: Start: 00210.79 End: 00212.79

Check Point @ 1205 hrs, 5.3 in H<sub>2</sub>O

Total Time:

Minutes  Mean Qa (m3/min)=

Laboratory Calculations:Filter Weights (grams):

Mean Qstd (m3/min)=  Final (Wf)   
 Vstd (m3)=  Initial (Wi)   
 TSP Concentration =  Net (Wn)

Formulas and Definitions

Mean Qstd =  $[(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})]^{1/2} - b)(1/m)$   
 Mean Qa = Mean Qstd(760/Pa)(Ta/298)  
 Vstd = (Qstd)\*(Total Time)  
 TSP Concentration (micrograms/m3) = (Wn)(10<sup>6</sup>)/Vstd  
 Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates  
 Pav & Tav = Daily Mean Baro. Pressure and Temperature  
 Mean Qa range must be 1.1 to 1.7 m3/min.

## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	08-04-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	WEST 6
<b>Operator:</b>	Sutphin	<b>Filter ID No.:</b>	Q0113415
<b>Pa (mm Hg)</b>	742.19	<b>Sampler S/N:</b>	0510
<b>Ta (°K)</b>	297.3	<b>Start Time:</b>	1330
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1530

## Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	5.4
Final Pex (in. H <sub>2</sub> O)	5.3
Mean Pex (in. H <sub>2</sub> O)	5.4

## Sampler:

## Regression Values

m=	1.4679
b=	0.0166
r=	0.9999

**Comments:** Elapsed Time; Start: 00212.79 End: 00214.79

Check Point @ 1433 hrs, 5.3 in H<sub>2</sub>O

## Total Time:

Minutes  Mean Qa (m3/min)=

## Laboratory Calculations:

## Filter Weights (grams):

Mean Qstd (m3/min)=  Final (Wf)   
 Vstd (m3)=  Initial (Wi)   
 TSP Concentration =  Net (Wn)

## Formulas and Definitions

$$\text{Mean Qstd} = [( \Delta P_{\text{ex}} ) ( P_a / 760 ) ( 298 / T_a ) ]^{1/2} - b ) ( 1 / m )$$

$$\text{Mean Qa} = \text{Mean Qstd} ( 760 / P_a ) ( T_a / 298 )$$

$$V_{\text{std}} = ( Q_{\text{std}} ) ( \text{Total Time} )$$

$$\text{TSP Concentration (micrograms/m}^3\text{)} = ( W_n ) ( 10^6 ) / V_{\text{std}}$$

Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates

Pav & Tav = Daily Mean Baro. Pressure and Temperature

Mean Qa range must be 1.1 to 1.7 m3/min.

TSP SAMPLER FIELD DATA SHEET			
<u>Installation:</u>	Anniston Army Depot	<u>Date:</u>	06-05-03
<u>Site ID:</u>	Crome Plating Facility	<u>Run Number:</u>	WEST 7
<u>Operator:</u>	Sulphin	<u>Filter ID No.:</u>	Q0113413
<u>Pa (mm Hg)</u>	745.24	<u>Sampler S/N:</u>	0510
<u>Ta (°K)</u>	294.3	<u>Start Time:</u>	0925
<u>Equip. Type:</u>	Graseby TSP Sampler	<u>Stop Time:</u>	1125
<u>Sampler Motor Manometer Readings:</u>		<u>Sampler:</u>	
Initial Pex (in. H <sub>2</sub> O)	5.3	<u>Regression Values</u>	
Final Pex (in. H <sub>2</sub> O)	5.2	m=	1.4679
Mean Pex (in. H <sub>2</sub> O)	5.3	b=	0.0166
		r=	0.9999
<u>Comments:</u> Elapsed Time; Start: 00214.79 End: 00216.79			
Check Point @ 1020 hrs, 5.2 in H <sub>2</sub> O			
<u>Total Time:</u>			
Minutes	120	Mean Qa (m3/min)=	1.555
<u>Laboratory Calculations:</u>		<u>Filter Weights (grams):</u>	
Mean Qstd (m3/min)=	1.54	Final (Wf)	N/A
Vstd (m3)=	185.29	Initial (Wi)	N/A
TSP Concentration =	N/A	Net (Wn)	N/A
<u>Formulas and Definitions</u>			
Mean Qstd = [(Delta Pex)(Pa/760)(298/Ta)] <sup>1/2</sup> -b)/(1/m)			
Mean Qa = Mean Qstd(760/Pa)(Ta/298)			
Vstd = (Qstd)*(Total Time)			
TSP Concentration (micrograms/m3) = (Wn)(10 <sup>6</sup> )/Vstd			
Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates			
Pav & Tav = Daily Mean Baro. Pressure and Temperature			
Mean Qa range must be 1.1 to 1.7 m3/min.			

## TSP SAMPLER FIELD DATA SHEET

<u>Installation:</u>	Anniston Army Depot	<u>Date:</u>	06-05-03
<u>Site ID:</u>	Crome Plating Facility	<u>Run Number:</u>	WEST 8
<u>Operator:</u>	Sutphin	<u>Filter ID No.:</u>	Q0113411
<u>Pa (mm Hg)</u>	745.49	<u>Sampler S/N:</u>	0510
<u>Ta (°K)</u>	296.8	<u>Start Time:</u>	1157
<u>Equip. Type:</u>	Graseby TSP Sampler	<u>Stop Time:</u>	1357

Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	5.3
Final Pex (in. H <sub>2</sub> O)	5.2
Mean Pex (in. H <sub>2</sub> O)	5.3

Sampler:Regression Values

m=	1.4679
b=	0.0166
r=	0.9999

Comments: Elapsed Time: Start: 00216.79 End: 00218.80

Check Point @ 1301 hrs, 5.2 in H<sub>2</sub>O

Total Time:

Minutes	120	<u>Mean Qa (m3/min)=</u>	1.561
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Laboratory Calculations:Filter Weights (grams):

<u>Mean Qstd (m3/min)=</u>	1.54	<u>Final (Wf)</u>	N/A
<u>Vstd (m3)=</u>	184.53	<u>Initial (Wi)</u>	N/A
<u>TSP Concentration =</u>	N/A	<u>Net (Wn)</u>	N/A

Formulas and Definitions

$$\text{Mean Qstd} = [(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})]^{1/2} \cdot b / (1/m)$$

$$\text{Mean Qa} = \text{Mean Qstd} (760/\text{Pa})(\text{Ta}/298)$$

$$\text{Vstd} = (\text{Qstd}) \cdot (\text{Total Time})$$

$$\text{TSP Concentration (micrograms/m3)} = (\text{Wn}) / (10^6) / \text{Vstd}$$

$$\text{Mean Qa \& Qstd} = \text{Mean Daily Actual \& Standard Flow Rates}$$

$$\text{Pav \& Tav} = \text{Daily Mean Baro. Pressure and Temperature}$$

$$\text{Mean Qa range must be 1.1 to 1.7 m3/min.}$$



## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-05-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	WEST 9
<b>Operator:</b>	Sutphin	<b>Filter ID No.</b>	Q0113409
<b>Pa (mm Hg)</b>	744.47	<b>Sampler S/N:</b>	0510
<b>Ta (°K)</b>	299.1	<b>Start Time:</b>	1425
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1625

## Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	5.2
Final Pex (in. H <sub>2</sub> O)	5.1
Mean Pex (in. H <sub>2</sub> O)	5.2

## Sampler:

## Regression Values

m=	1.4679
b=	0.0166
r=	0.9999

**Comments:** Elapsed Time; Start: 00218.80 End: 00220.81

Check Point @ 1530 hrs, 5.1 in H<sub>2</sub>O

## Total Time:

Minutes  Mean Qa (m3/min)=

## Laboratory Calculations:

Mean Qstd (m3/min)=

Vstd (m3)=

TSP Concentration =

## Filter Weights (grams):

Final (Wf)

Initial (Wi)

Net (Wn)

## Formulas and Definitions

$$\text{Mean Qstd} = [(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})^{1/2} - b](1/m)$$

$$\text{Mean Qa} = \text{Mean Qstd}(760/\text{Pa})(\text{Ta}/298)$$

$$\text{Vstd} = (\text{Qstd}) \times (\text{Total Time})$$

$$\text{TSP Concentration (micrograms/m}^3\text{)} = (\text{Wn})(10^6)/\text{Vstd}$$

Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates

Pav & Tav = Daily Mean Baro. Pressure and Temperature

Mean Qa range must be 1.1 to 1.7 m3/min.



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TSP SAMPLER EAST FIELD DATA SHEET

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## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-03-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	EAST 1
<b>Operator:</b>	Sutphin	<b>Filter ID No.:</b>	Q0113426
<b>Pa (mm Hg)</b>	740.41	<b>Sampler S/N:</b>	6631
<b>Ta (°K)</b>	297.9	<b>Start Time:</b>	1113
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1311

## Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	6.1
Final Pex (in. H <sub>2</sub> O)	5.9
Mean Pex (in. H <sub>2</sub> O)	6.00

## Sampler:

## Regression Values

m=	1.5247
b=	0.1084
r=	0.0000

Comments: Elapsed Time; Start: 00596.26 End: 00598.22

Check Point @ 1209 hrs, 5.9 in H<sub>2</sub>O

## Total Time:

Minutes	118	Mean Qa (m3/min)=	1.554
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## Laboratory Calculations:

## Filter Weights (grams):

Mean Qstd (m3/min)=	1.51	Final (Wf)	N/A
Vstd (m3)=	178.75	Initial (Wi)	N/A
TSP Concentration =	N/A	Net (Wn)	N/A

## Formulas and Definitions

$\text{Mean Qstd} = [(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})]^{1/2} - b)(1/m)$   
 $\text{Mean Qa} = \text{Mean Qstd}(760/\text{Pa})(\text{Ta}/298)$   
 $\text{Vstd} = (\text{Qstd})(\text{Total Time})$   
 $\text{TSP Concentration (micrograms/m3)} = (\text{Wn})(10^6)/\text{Vstd}$   
 $\text{Mean Qa \& Qstd} = \text{Mean Daily Actual \& Standard Flow Rates}$   
 $\text{Pav \& Tav} = \text{Daily Mean Baro. Pressure and Temperature}$   
 $\text{Mean Qa range must be 1.1 to 1.7 m3/min.}$

## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-03-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	EAST 2
<b>Operator:</b>	Sutphin	<b>Filter ID No.:</b>	Q0113424
<b>Pa (mm Hg)</b>	740.16	<b>Sampler S/N:</b>	6631
<b>Ta (°K)</b>	297.7	<b>Start Time:</b>	1424
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1623

## Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	6.0
Final Pex (in. H <sub>2</sub> O)	5.8
Mean Pex (in. H <sub>2</sub> O)	5.9

## Sampler:

## Regression Values

m=	1.5247
b=	0.1084
r=	0.9999

**Comments:** Elapsed Time; Start: 00598.23 End: 00600.22

Check Point @ 1521 hrs, 5.9 in H<sub>2</sub>O

## Total Time:

Minutes  Mean Qa (m<sup>3</sup>/min)=

## Laboratory Calculations:

Mean Qstd (m<sup>3</sup>/min)=

Vstd (m<sup>3</sup>)=

TSP Concentration =

## Filter Weights (grams):

Final (Wf)

Initial (Wi)

Net (Wn)

## Formulas and Definitions

Mean Qstd = [(Delta Pex)(Pa/760)(298/Ta)]<sup>1/2</sup> - b)(1/m)

Mean Qa = Mean Qstd(760/Pa)(Ta/298)

Vstd = (Qstd)\*(Total Time)

TSP Concentration (micrograms/m<sup>3</sup>) = (Wn)(10<sup>6</sup>)/Vstd

Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates

Pav & Tav = Daily Mean Baro. Pressure and Temperature

Mean Qa range must be 1.1 to 1.7 m<sup>3</sup>/min.

## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-03-03
<b>Site ID:</b>	Chrome Plating Facility	<b>Run Number:</b>	EAST 3
<b>Operator:</b>	Sutphin	<b>Filter ID No.:</b>	Q0113422
<b>Pa (mm Hg)</b>	739.89	<b>Sampler S/N:</b>	6631
<b>Ta (°K)</b>	298	<b>Start Time:</b>	1702
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1903

## Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	6.0
Final Pex (in. H <sub>2</sub> O)	5.8
Mean Pex (in. H <sub>2</sub> O)	5.9

## Sampler:

## Regression Values

m=	1.5247
b=	0.1084
r=	0.9999

Comments: Elapsed Time; Start: 00600.23 End: 00602.23

Check Point @ 1806 hrs, 5.8 in H<sub>2</sub>O

## Total Time:

Minutes

121

Mean Qa (m<sup>3</sup>/min)=

1.542

## Laboratory Calculations:

## Filter Weights (grams):

Mean Qstd (m<sup>3</sup>/min)=

1.50

Final (Wf)

N/A

Vstd (m<sup>3</sup>)=

181.59

Initial (Wi)

N/A

TSP Concentration =

N/A

Net (Wn)

N/A

## Formulas and Definitions

Mean Qstd = [(Delta Pex)(Pa/760)(298/Ta)]<sup>1/2</sup> - b)(1/m)

Mean Qa = Mean Qstd(760/Pa)(Ta/298)

Vstd = (Qstd)\*(Total Time)

TSP Concentration (micrograms/m<sup>3</sup>) = (Wn)(10<sup>6</sup>)/Vstd

Mean Qa &amp; Qstd = Mean Daily Actual &amp; Standard Flow Rates

Pav &amp; Tav = Daily Mean Baro. Pressure and Temperature

Mean Qa range must be 1.1 to 1.7 m<sup>3</sup>/min.

## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-04-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	EAST 4
<b>Operator:</b>	Sutphin	<b>Filter ID No.</b>	Q0113420
<b>Pa (mm Hg)</b>	741.43	<b>Sampler S/N:</b>	6631
<b>Ta (°K)</b>	294.5	<b>Start Time:</b>	0826
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1027

## Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	5.9
Final Pex (in. H <sub>2</sub> O)	5.9
Mean Pex (in. H <sub>2</sub> O)	5.9

## Sampler:

## Regression Values

m=	1.5247
b=	0.1084
r=	0.9999

**Comments:** Elapsed Time: Start: 00602.23 End: 00604.24

Check Point @ 0927 hrs, 5.9 in H<sub>2</sub>O

## Total Time:

Minutes  Mean Qa (m3/min)=

## Laboratory Calculations:

## Filter Weights (grams):

Mean Qstd (m3/min)=  Final (Wf)   
 Vstd (m3)=  Initial (Wi)   
 TSP Concentration =  Net (Wn)

## Formulas and Definitions

Mean Qstd =  $[(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})]^{1/2} - b)(1/m)$   
 Mean Qa = Mean Qstd(760/Pa)(Ta/298)  
 Vstd = (Qstd)\*(Total Time)  
 TSP Concentration (micrograms/m3) = (Wn)/(10<sup>6</sup>)/Vstd  
 Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates  
 Pav & Tav = Daily Mean Baro. Pressure and Temperature  
 Mean Qa range must be 1.1 to 1.7 m3/min.



TSP SAMPLE SHEET	
<b>Installation:</b> Anniston <b>Site ID:</b> Cromie Pla <b>Operator:</b> Su <b>Pa (mm Hg)</b> <b>Ta (°K)</b> <b>Equip. Type:</b> Graseby TSP Sampler	<b>Date:</b> 06-04-03 <b>Station Number:</b> EAST 5 <b>Filter ID No.</b> Q0113418 <b>Sampler S/N:</b> 6631 <b>Start Time:</b> 1106 <b>Stop Time:</b> 1306
<b>Sampler Motor Manometer Readings:</b>	
<b>Initial Pex (in. H<sub>2</sub>O)</b> 5.9 <b>Final Pex (in. H<sub>2</sub>O)</b> 5.9 <b>Mean Pex (in. H<sub>2</sub>O)</b> 5.9	<b>Sampler:</b> <b>Regression Values</b> <b>m=</b> 1.5247 <b>b=</b> 0.1084 <b>r=</b> 0.9999
<b>Comments:</b> Elapsed Time; Start: 00604.24 End: 00606.25 Check Point @ 1206 hrs, 5.9 in H <sub>2</sub> O	
<b>Total Time:</b> Minutes 120 <b>Mean Qa (m<sup>3</sup>/min)=</b> 1.531	
<b>Laboratory Calculations:</b>	
<b>Mean Qstd (m<sup>3</sup>/min)=</b> 1.51 <b>Vstd (m<sup>3</sup>)=</b> 181.47 <b>TSP Concentration =</b> N/A	<b>Filter Weights (grams):</b> <b>Final (Wf)</b> N/A <b>Initial (Wi)</b> N/A <b>Net (Wn)</b> N/A
<b>Formulas and Definitions</b>	
$\text{Mean Qstd} = [(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})]^{1/2} \cdot b \cdot (1/m)$ $\text{Mean Qa} = \text{Mean Qstd}(760/\text{Pa})(\text{Ta}/298)$ $\text{Vstd} = (\text{Qstd}) \cdot (\text{Total Time})$ $\text{TSP Concentration (micrograms/m}^3\text{)} = (\text{Wn})(10^6)/\text{Vstd}$ $\text{Mean Qa \& Qstd} = \text{Mean Daily Actual \& Standard Flow Rates}$ $\text{Pav \& Tav} = \text{Daily Mean Baro. Pressure and Temperature}$ Mean Qa range must be 1.1 to 1.7 m <sup>3</sup> /min.	

TSP SAMP		SHEET	
Installation:	Anniston	Date:	06-04-03
Site ID:	Crome Pla	Station Number:	EAST 6
Operator:	Su	Filter ID No.	Q0113414
Pa (mm Hg)		Sampler S/N:	6631
Ta (°K)		Start Time:	1331
Equip. Type:	Graseby TSP Sampler	Stop Time:	1531
<b>Sampler Motor Manometer Readings:</b>		<b>Sampler:</b>	
Initial Pex (in. H <sub>2</sub> O)	5.9	<b>Regression Values</b>	
Final Pex (in. H <sub>2</sub> O)	5.8	m=	1.5247
Mean Pex (in. H <sub>2</sub> O)	5.9	b=	0.1084
		r=	0.9999
Comments: Elapsed Time; Start: 00606.25 End: 00608.25			
Check Point @ 1435 hrs, 5.8 in H <sub>2</sub> O			
<b>Total Time:</b>			
Minutes	120	Mean Qa (m <sup>3</sup> /min)=	1.531
<b>Laboratory Calculations:</b>		<b>Filter Weights (grams):</b>	
Mean Qstd (m <sup>3</sup> /min)=	1.50	Final (Wf)	N/A
Vstd (m <sup>3</sup> )=	179.81	Initial (Wi)	N/A
TSP Concentration =	N/A	Net (Wn)	N/A
<b>Formulas and Definitions</b>			
Mean Qstd = [(Delta Pex)(Pa/760)(298/Ta)] <sup>1/2</sup> -b)(1/m)			
Mean Qa = Mean Qstd(760/Pa)(Ta/298)			
Vstd = (Qstd)*(Total Time)			
TSP Concentration (micrograms/m <sup>3</sup> ) = (Wn)(10 <sup>6</sup> )/Vstd			
Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates			
Pav & Tav = Daily Mean Baro. Pressure and Temperature			
Mean Qa range must be 1.1 to 1.7 m <sup>3</sup> /min.			

## TSP SAMPLER FIELD DATA SHEET

<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-05-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	EAST 7
<b>Operator:</b>	Sutphin	<b>Filter ID No.</b>	Q0113412
<b>Pa (mm Hg)</b>	745.24	<b>Sampler S/N:</b>	6631
<b>Ta (°K)</b>	204.3	<b>Start Time:</b>	0926
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1126

## Sampler Motor Manometer Readings:

Initial Pex (In. H <sub>2</sub> O)	6.0
Final Pex (In. H <sub>2</sub> O)	6.1
Mean Pex (In. H <sub>2</sub> O)	6.1

## Sampler:

## Regression Values

m=	1.5247
b=	0.1084
r=	0.9999

**Comments:** Elapsed Time; Start: 00608.25 End: 00610.26

Check Point @ 1022 hrs, 6.1 in H<sub>2</sub>O

## Total Time:

Minutes  Mean Qa (m3/min)=

## Laboratory Calculations:

## Filter Weights (grams):

Mean Qstd (m3/min)=	<input type="text" value="1.54"/>	Final (Wf)	<input type="text" value="N/A"/>
Vstd (m3)=	<input type="text" value="184.37"/>	Initial (Wi)	<input type="text" value="N/A"/>
TSP Concentration =	<input type="text" value="N/A"/>	Net (Wn)	<input type="text" value="N/A"/>

## Formulas and Definitions

$$\text{Mean Qstd} = \left[ \frac{(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})}{1} - b \right] (1/m)$$

$$\text{Mean Qa} = \text{Mean Qstd} (760/\text{Pa})(\text{Ta}/298)$$

$$\text{Vstd} = (\text{Qstd}) * (\text{Total Time})$$

$$\text{TSP Concentration (micrograms/m}^3\text{)} = (\text{Wn})(10^6)/\text{Vstd}$$

$$\text{Mean Qa \& Qstd} = \text{Mean Daily Actual \& Standard Flow Rates}$$

$$\text{Pav \& Tav} = \text{Daily Mean Baro. Pressure and Temperature}$$

$$\text{Mean Qa range must be 1.1 to 1.7 m}^3\text{/min.}$$

## TSP SAMPLER FIELD DATA SHEET

<u>Installation:</u>	Anniston Army Depot	<u>Date:</u>	08-05-03
<u>Site ID:</u>	Crome Plating Facility	<u>Run Number:</u>	EAST 8
<u>Operator:</u>	Sutphin	<u>Filter ID No.</u>	Q0113410
<u>Pa (mm Hg)</u>	745.49	<u>Sampler S/N:</u>	6631
<u>Ta (°K)</u>	296.8	<u>Start Time:</u>	1157
<u>Equip. Type:</u>	Graseby TSP Sampler	<u>Stop Time:</u>	1357

## Sampler Motor Manometer Readings:

Initial Pex (in. H <sub>2</sub> O)	6.1
Final Pex (in. H <sub>2</sub> O)	6.0
Mean Pex (in. H <sub>2</sub> O)	6.1

## Sampler:

## Regression Values

m=	1.5247
b=	0.1084
r=	0.9999

Comments: Elapsed Time; Start: 00610.26 End: 00612.26

Check Point @ 1302 hrs, 6.0 in H<sub>2</sub>O

## Total Time:

Minutes  Mean Qa (m<sup>3</sup>/min)=

## Laboratory Calculations:

## Filter Weights (grams):

Mean Qstd (m <sup>3</sup> /min)=	<input type="text" value="1.53"/>	Final (Wf)	<input type="text" value="N/A"/>
Vstd (m <sup>3</sup> )=	<input type="text" value="183.59"/>	Initial (Wi)	<input type="text" value="N/A"/>
TSP Concentration =	<input type="text" value="N/A"/>	Net (Wn)	<input type="text" value="N/A"/>

## Formulas and Definitions

$$\text{Mean Qstd} = [(\Delta \text{Pex})(\text{Pa}/760)(298/\text{Ta})]^{1/2} - b)(1/m)$$

$$\text{Mean Qa} = \text{Mean Qstd}(760/\text{Pa})(\text{Ta}/298)$$

$$\text{Vstd} = (\text{Qstd})(\text{Total Time})$$

$$\text{TSP Concentration (micrograms/m}^3) = (\text{Wn})(10^6)/\text{Vstd}$$

$$\text{Mean Qa \& Qstd} = \text{Mean Daily Actual \& Standard Flow Rates}$$

$$\text{Pav \& Tav} = \text{Daily Mean Baro. Pressure and Temperature}$$

$$\text{Mean Qa range must be 1.1 to 1.7 m}^3/\text{min.}$$



TSP SAMPLER FIELD DATA SHEET			
<b>Installation:</b>	Anniston Army Depot	<b>Date:</b>	06-05-03
<b>Site ID:</b>	Crome Plating Facility	<b>Run Number:</b>	EAST 9
<b>Operator:</b>	Sutphin	<b>Filter ID No.</b>	Q0113408
<b>Pa (mm Hg)</b>	744.47	<b>Sampler S/N:</b>	6631
<b>Ta (°K)</b>	299.1	<b>Start Time:</b>	1426
<b>Equip. Type:</b>	Graseby TSP Sampler	<b>Stop Time:</b>	1627

<b>Sampler Motor Manometer Readings:</b>	<b>Sampler:</b>												
<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 60%;">Initial Pex (in. H<sub>2</sub>O)</td> <td style="width: 40%;">5.9</td> </tr> <tr> <td>Final Pex (in. H<sub>2</sub>O)</td> <td>5.9</td> </tr> <tr> <td>Mean Pex (in. H<sub>2</sub>O)</td> <td>5.9</td> </tr> </table>	Initial Pex (in. H <sub>2</sub> O)	5.9	Final Pex (in. H <sub>2</sub> O)	5.9	Mean Pex (in. H <sub>2</sub> O)	5.9	<b>Regression Values</b> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 60%;">m=</td> <td style="width: 40%;">1.5247</td> </tr> <tr> <td>b=</td> <td>0.1084</td> </tr> <tr> <td>r=</td> <td>0.9999</td> </tr> </table>	m=	1.5247	b=	0.1084	r=	0.9999
Initial Pex (in. H <sub>2</sub> O)	5.9												
Final Pex (in. H <sub>2</sub> O)	5.9												
Mean Pex (in. H <sub>2</sub> O)	5.9												
m=	1.5247												
b=	0.1084												
r=	0.9999												

**Comments:** Elapsed Time: Start: 00610.26 End: 00612.26

Check Point @ 1302 hrs, 6.0 in H<sub>2</sub>O

<b>Total Time:</b>	
Minutes	121
<b>Mean Qa (m<sup>3</sup>/min)=</b>	1.540

<b>Laboratory Calculations:</b>	<b>Filter Weights (grams):</b>
<b>Mean Qstd (m<sup>3</sup>/min)=</b>	1.50
<b>Vstd (m<sup>3</sup>)=</b>	181.83
<b>TSP Concentration =</b>	N/A
<b>Final (Wf)</b>	N/A
<b>Initial (Wi)</b>	N/A
<b>Net (Wn)</b>	N/A

**Formulas and Definitions**

Mean Qstd = [(Delta Pex)(Pa/760)(298/Ta)]<sup>1/2</sup> - b)(1/m)

Mean Qa = Mean Qstd(760/Pa)(Ta/298)

Vstd = (Qstd)\*(Total Time)

TSP Concentration (micrograms/m<sup>3</sup>) = (Wn)(10<sup>6</sup>)/Vstd

Mean Qa & Qstd = Mean Daily Actual & Standard Flow Rates

Pav & Tav = Daily Mean Baro. Pressure and Temperature

Mean Qa range must be 1.1 to 1.7 m<sup>3</sup>/min.



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

APPENDIX H  
ANALYTICAL PACKAGE

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Air Pollution Management Study No. 43-EL-5116-03,

USEPA RM 306 ANALYTICAL PACKAGE

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**CASE NARRATIVE****STL SACRAMENTO PROJECT NUMBER G3F110295**

There were no anomalies associated with this project.

*STL Sacramento*  
Quality Control Definitions

QC Parameter	Definition
QC Batch	A set of up to 20 field samples plus associated laboratory QC samples that are similar in composition (matrix) and that are processed within the same time period with the same reagent and standard lots.
Duplicate Control Sample (DCS)	Consist of a pair of LCSs analyzed within the same QC batch to monitor precision and accuracy independent of sample matrix effects. This QC is performed only if required by client or when insufficient sample is available to perform MS/MSD.
Duplicate Sample (DU)	A second aliquot of an environmental sample, taken from the same sample container when possible, that is processed independently with the first sample aliquot. The results are used to assess the effect of the sample matrix on the precision of the analytical process. The precision estimated using this sample is not necessarily representative of the precision for other samples in the batch.
Laboratory Control Sample (LCS)	A volume of reagent water for aqueous samples or a contaminant-free solid matrix (Ottawa sand) for soil and sediment samples which is spiked with known amounts of representative target analytes and required surrogates. An LCS is carried through the entire analytical process and is used to monitor the accuracy of the analytical process independent of potential matrix effects.
Matrix Spike and Matrix Spike Duplicate (MS/MSD)	A field sample fortified with known quantities of target analytes that are also added to the LCS. Matrix spike duplicate is a second matrix spike sample. MSs/MSDs are carried through the entire analytical process and are used to determine sample matrix effect on accuracy of the measurement system. The accuracy and precision estimated using MS/MSD is only representative of the precision of the sample that was spiked.
Method Blank (MB)	A sample composed of all the reagents (in the same quantities) in reagent water carried through the entire analytical process. The method blank is used to monitor the level of contamination introduced during sample preparation steps.
Surrogate Spike	Organic constituents not expected to be detected in environmental media and are added to every sample and QC at a known concentration. Surrogates are used to determine the efficiency of the sample preparation and the analytical process.

Source: STL Sacramento Laboratory Quality Manual

**STL Sacramento Certifications:**

Alaska (UST-055), Arizona (#A200616), Arkansas, California (NELAP # 01119CA) (ELAP #I-2439), Connecticut (#PH-0691), Florida (E87570), Hawaii, Louisiana (AI # 30612), New Jersey (Lgb ID 44005), Nevada (#CA 044), New York (LAB ID 11666 serial # 107407), Oregon (LAB ID CA 044), South Carolina (LAB ID 87014, Cert. # 870140), Utah (E-168), Virginia (#00178), Washington (# C087), West Virginia (# 9930C), Wisconsin (Lab 998204680), USNAVY, USACE, USDA Foreign Plant (Permit # 37-82605), USDA Foreign Soil (Permit # S-46613).

## Sample Summary G3F110295

WO#	Sample #	Client Sample ID	Sampling Date	Received Date
FQC6G	1	43ANAD001 DLS8455001	6/3/03	6/11/03 09:05 AM
FQC6G	1	43ANAD001 DLS8455001 DUP	6/3/03	6/11/03 09:05 AM
FQC6V	2	43ANAD004 DLS8455002	6/3/03	6/11/03 09:05 AM
FQC65	3	43ANAD007 DLS8455003	6/3/03	6/11/03 09:05 AM
FQC67	4	43ANAD013 DLS8455004	6/4/03	6/11/03 09:05 AM
FQC69	5	43ANAD016 DLS8455005	6/4/03	6/11/03 09:05 AM
FQC7C	6	43ANAD019 DLS8455018	6/4/03	6/11/03 09:05 AM
FQC7G	7	43ANAD023 DLS8455019	6/5/03	6/11/03 09:05 AM
FQC7H	8	43ANAD026 DLS8455020	6/5/03	6/11/03 09:05 AM
FQC7P	9	43ANAD029 DLS8455021	6/5/03	6/11/03 09:05 AM
FQC7T	10	43ANAD010 DLS8455031	6/3/03	6/11/03 09:05 AM
FQC70	11	43ANAD022 DLS8455032	6/4/03	6/11/03 09:05 AM
FQC71	12	43ANAD032 DLS8455033	6/5/03	6/11/03 09:05 AM

### Notes(s):

- The analytical results of the samples listed above are presented on the following pages.
- All calculations are performed before rounding to avoid round-off errors in calculated results.
- Results noted as "ND" were not detected at or above the stated limit.
- This report must not be reproduced, except in full, without the written approval of the laboratory.
- Results for the following parameters are never reported on a dry weight basis: color, corrosivity, density, flashpoint, ignitability, layers, odor, paint filter test, pH, porosity, pressure, reactivity, redox potential, specific gravity, spot tests, solids, solubility, temperature, viscosity, and weight



AIR, 306/6020, Chromium

## UNCLASSIFIED

Client Sample ID: 43ANAD001 DLS#455001

## TOTAL Metals

Lot-Sample #...: G3F110295-D01

Matrix.....: AIR

Date Sampled...: 06/03/03

Date Received...: 06/11/03

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
Prep Batch #...: 3170438						
Chromium	34.2 J	1.0	ug	SW846 6020	06/17-06/25/03	PQC6G1AA
		Dilution Factor: 1		MDL.....: 0.46		

## NOTE(S):

J Method Blank concentration. The associated method blank contains the target analyte at a reportable level.

Client Sample ID: 43ANAD004 DLS8455002

## TOTAL Metals

Lot-Sample #: G3F110295-002

Matrix.....: AIR

Date Sampled...: 06/03/03

Date Received...: 06/11/03

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
Prep Batch #...	3170438					
Chromium	20.4 J	0.90	ug	SW846 6020	06/17-06/25/03	PQCEVLAA
		Dilution Factor: 1		MDL.....: 0.41		

## NOTE(s):

J: Method blank contamination. The associated method blank contains the target analyte at a reportable level.

## UNCLASSIFIED

Client Sample ID: 43AMAD007 DLS8455003

## TOTAL Metals

Lot-Sample #...: G3F110295-003

Matrix.....: AIR

Date Sampled...: 06/03/03

Date Received...: 06/11/03

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
Prep Batch #...: 3170438						
Chromium	14.5 J	0.90	ug	SW846 6020	06/17-06/25/03	PQC651AA
		Dilution Factor: 1		MDL.....: 0.41		

NOTE(E):

J Method blank concentration. The associated method blank contains the target analyte at a reportable level.

UNCLASSIFIED

Client Sample ID: 43ANAD013 DLG8455004

## TOTAL Metals

Lot-Sample #...: G3F110295-004

Matrix.....: AIR

Date Sampled...: 06/04/03

Date Received...: 06/11/03

PARAMETER	RESULT	REPORTING		METHOD	PREPARATION-	WORK
		LIMIT	UNITS		ANALYSIS DATE	ORDER #
Prep Batch #...: 3170438						
Chromium	25.2 J	0.90	ug	SW846 6020	06/17-06/25/03	PQC671AA
		Dilution Factor: 1		MDL.....: 0.41		

## NOTE(S):

J Method blank contamination. The associated method blank contains the target analyte at a reportable level.



UNPL-11177

Client Sample ID: 43ANAD016 DLS8455005

## TOTAL Metals

Lot-Sample #...: G3F110295-005

Matrix.....: AIR

Date Sampled...: 06/04/03

Date Received...: 06/11/03

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
Prep Batch #...: 3170438						
Chromium	9.2 J	0.89	ug	SW846 6020	06/17-06/25/03	FQC691AA
		Dilution Factor: 1		MDL.....: 0.41		

## NOTE(S):

J Method blank contamination. The associated method blank contains the target analyte at a reportable level.

Client Sample ID: 43ANAD019 DLS8455018

## TOTAL Metals

Lot-Sample #...: G3F110295-006  
Date Sampled...: 06/04/03

Date Received...: 06/11/03

Matrix.....: AIR

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
Prep Batch #...	3170438					
Chromium	17.9 J	0.90	ug	SW845 6020	06/17-06/25/03	FQC7CLAA
		Dilution Factor: 1		MDL.....: 0.41		

## NOTE(S):

J Method blank contamination. The associated method blank contains the target analyte at a reportable level.

Client Sample ID: 43ANAD023 DLS8455019

## TOTAL Metals

Lot-Sample #: G3F110295-007

Matrix: AIR

Date Sampled: 06/05/03

Date Received: 06/11/03

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
Prep Batch #	3170438					
Chromium	31.7 J	0.90	ug	SW846 6020	06/17-06/25/03	POC7G1AA
		Dilution Factor: 1		MDL: 0.41		

## NOTE(S):

1 Method blank contamination. The associated method blank contains the target analyte at a reportable level.

LH500-000000 0.075

Client Sample ID: 43ANAD026 DLS8455020

## TOTAL Metals

Lot-Sample #: G3F110295-006

Matrix: AIR

Date Sampled: 06/05/03

Date Received: 06/11/03

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
Prep Batch #	3170438					
Chromium	30.0 J	0.90	ug	SW846 6020	06/17-06/25/03	FQC7H1AA
		Dilution Factor: 1		MDL: 0.41		

## NOTE(S):

J Method blank concentration. The associated method blank contains the target analyte at a reportable level.

Client Sample ID: 43ANAD029 DE8455021

TOTAL Metals

Lot-Sample #...: G3F110295-009

Matrix.....: AIR

Date Sampled...: 06/05/03

Date Received...: 06/11/03

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
Prop Batch #...: 3170438						
Chromium	34.2 J	0.90	ug	SW846 6020	06/17-06/25/03	PQC7PLAA
		Dilution Factor: 1		MDL.....: 0.41		

NOTE(S):

J Method blank contamination. The associated method blank contains the target analyte at a reportable level.



## UNCLASSIFIED

Client Sample ID: 43ANAD010 DLS8455031

## TOTAL Metals

Lot-Sample #...: G3F110295-010

Matrix.....: AIR

Date Sampled...: 06/03/03

Date Received...: 06/11/03

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
Prep Batch #...	3170438					
Chromium	0.66 B,J	0.99	ug	SW846 6020	06/17-06/25/03	PQC7T1AA
		Dilution Factor: 1		MEL.....: 0.46		

## NOTE(S):

B Refracted result. Result is less than EL.

J Method blank contamination. The associated method blank contains the target analyte at a reportable level.

Client Sample ID: 43ANAD022 DLS8455032

## TOTAL Metals

Lot-Sample #...: G3F110295-011

Matrix.....: AIR

Date Sampled...: 06/04/03

Date Received...: 06/11/03

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
Prep Batch #...: 3170438						
Chromium	0.76 B,J	0.99	ug	SW846 6020	06/17-06/25/03	FQC701AA
		Dilution Factor: 1		MDL.....: 0.46		

## NOTE(S):

B Estimated result. Result is less than RL.

J Method Blank contamination. The associated method blank contains the target analyte at a reportable level.

Client Sample ID: 43ANAD032 DLS8455033

## TOTAL Metals

Lot-Sample #....: G3F110295-012

Matrix.....: AIR

Date Sampled....: 06/05/03

Date Received...: 06/11/03

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER
Prep Batch #....: 3170438						
Chromium	1.1 J	0.99	ug	SWS46 6020	06/17-06/25/03	POC711
		Dilution Factor: 1		MDL.....: 0.46		

## NOTE(S):

J Method blank contamination. The associated method blank contains the target analyte at a reportable level.

**QC DATA ASSOCIATION SUMMARY**

G3F110295

## Sample Preparation and Analysis Control Numbers

<u>SAMPLE#</u>	<u>MATRIX</u>	<u>ANALYTICAL METHOD</u>	<u>LEACH BATCH #</u>	<u>PREP BATCH #</u>	<u>MS RUN#</u>
001	AIR	SW846 6020		3170438	3170181
002	AIR	SW846 6020		3170438	3170181
003	AIR	SW846 6020		3170438	3170181
004	AIR	SW846 6020		3170438	3170181
005	AIR	SW846 6020		3170438	3170181
006	AIR	SW846 6020		3170438	3170181
007	AIR	SW846 6020		3170438	3170181
008	AIR	SW846 6020		3170438	3170181
009	AIR	SW846 6020		3170438	3170181
010	AIR	SW846 6020		3170438	3170181
011	AIR	SW846 6020		3170438	3170181
012	AIR	SW846 6020		3170438	3170181

## METHOD BLANK REPORT

## TOTAL Metals

Client Lot #...: G3F110295

Matrix.....: AIR

PARAMETER	RESULT	REPORTING LIMIT	UNITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
MB Lot-Sample #: G3F190000-438 Prep Batch #...: 3170438						
Chromium	0.43 B	0.89	ug	SW846 6020	06/17-06/25/03	FQVFS1AA

## NOTE(S):

Calculations are performed before rounding to avoid round-off errors in calculated results.

B - Estimated result. Result is less than RL.



## LABORATORY CONTROL SAMPLE DATA REPORT

## TOTAL Metals

Lot-Sample #...: G3F110295

Matrix.....: AIR

PARAMETER	SPIKE AMOUNT	MEASURED AMOUNT	UNITS	PERCENT RECOVERY	RPD	METHOD	PREPARATION- ANALYSIS DATE	PREP BATCH #
Chromium	89.0	87.5	ug	98		SW846 6020	06/17-06/25/03	3170438
	89.0	86.5	ug	97	1.2	SW846 6020	06/17-06/25/03	3170438

## NOTE(S):

Calculations are performed before rounding to avoid round-off errors in calculated results.

## LABORATORY CONTROL SAMPLE EVALUATION REPORT

## TOTAL Metals

Lot-Sample #...: G3F110295

Matrix.....: AIR

PARAMETER	PERCENT RECOVERY	RECOVERY LIMITS	RPD RPD	LIMITS	METHOD	PREPARATION- ANALYSIS DATE	PREP- BATCH #
Chromium	98	(82 - 119)			SW846 6020	06/17-06/25/03	3170438
	97	(82 - 119)	1.2	(0-20)	SW846 6020	06/17-06/25/03	3170438

## NOTE (S) :

Calculations are performed before rounding to avoid round-off errors in calculated results.

## MATRIX SPIKE SAMPLE DATA REPORT

## TOTAL Metals

Client Lot #...: G3F110295  
Date Sampled...: 06/03/03

Date Received...: 06/11/03

Matrix.....: AIR

PARAMETER	SAMPLE AMOUNT	SPIKE AMT	MEASURED AMOUNT	UNITS	PERCENT RECOVERY	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
MS Lot-Sample #: G3F110295-001 Prep Batch #...: 3170438								
Chromium	34.2	100	129	ug	94	SW846 6020	06/17-06/25/03	FQC6G1AC

## NOTE(S):

Calculations are performed before rounding to avoid round-off errors in calculated results.

## MATRIX SPIKE SAMPLE EVALUATION REPORT

## TOTAL Metals

Client Lot #...: G3F110295

Matrix.....: AIR

Date Sampled...: 06/03/03

Date Received...: 06/11/03

PARAMETER	PERCENT RECOVERY	RECOVERY LIMITS	METHOD	PREPARATION- ANALYSIS DATE	WORK ORDER #
MS Lot-Sample #: G3F110295-001			Prep Batch #...: 3170438		
Chromium	94	(82 - 119)	SW846 6020	06/17-06/25/03	PQCEGLAC

## NOTE(S):

Calculations are performed before rounding to avoid round-off errors in calculated results.

# SAMPLE DUPLICATE EVALUATION REPORT

## Metale

Client Lot #...: G3F110295

Work Order #...: PQC6G-SMP

Matrix.....: ATR

FQC6G-DUP

Date Sampled...: 06/03/03

Date Received.: 06/11/03

PARAM	RESULT	DUPLICATE RESULT	UNITS	RPD	RPD LIMIT	METHOD	PREPARATION- ANALYSIS DATE	PREP BATCH #
Chromium	34.2 J	35.6	ug	3.9	(0-20)	SD Lot-Sample #: SW846 6020	G3F110295-001 06/17-06/25/03	3170438

NOTE(S) :

Calculations are performed before rounding to avoid round-off errors in calculated results.

**J Method blank contamination.** The associated method blank contains the target analyte at a reportable level.

Air Pollution Management Study No. 03-EL-5116-03, 3-1

TSP SAMPLER ANALYTICAL PACKAGE

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CASE NARRATIVE  
Microbac Laboratories, Inc., Gascoyne Division

Report Number: 0306390

July 8, 2003

Report To: U.S. Army Center for Health Promotion and  
Preventive Medicine (USACHPPM)  
Aberdeen Proving Ground, MD 21010-5422  
Project #DAAD05-01-D-0006      Metals

page 1 of 1

Pick-Up Order: 051/3

Date Samples Received: 06/17/03

Sample Numbers: 8455006 - 8455017, 8455022 - 8455030

Matrix: Air Filter

Twenty-one samples were transported to Microbac Laboratories, Inc., Gascoyne Division via laboratory courier and were relinquished to lab personnel in the sample control department for log-in. The sample containers were checked and were noted to be in satisfactory condition. The Field ID for sample 8455025 was incorrectly identified on the Pick-up Order, compared to the sample container. The USACHPPM COR was notified and the laboratory was instructed to correct the ID on the paperwork.

Requested test parameters performed by Microbac Laboratories, Inc., Gascoyne Division:

\* Metals analysis, using EPA SW-846 methodology

## References:

Test Methods for Evaluating Solid Waste, SW-846, Third Edition, Office of Solid Waste and Emergency Response, USEPA, Wash.,DC, November 1986; Final Update I, July 1992 Final Update II, September 1994 Final Update III, December 1996

NOTE: Exceptions to the requested test parameters are as follows: The requested analysis on the Pick-up Order was EPA 200.8. Since the samples were air filters, the USACHPPM COR was notified and the laboratory was instructed to change the requested test to EPA 6020.

All laboratory quality control parameters were met with the following exceptions:

1. The concentrations of the Matrix Spike and Matrix Spike Duplicate (0306390-001 8455006) were inappropriate compared to the native concentration in the sample. The sample was diluted and reanalyzed. Recoveries of Post Digestion Spikes were acceptable.

Enclosed are the following:

1. Report of Analysis (original plus one copy)
2. Chain-of-Custody (original plus one copy)
3. Pick-Up Order/Delivery Order (original plus one copy)
4. Laboratory Chronicle / Case Narrative (original plus one copy)
5. Quality Control Summary Report (original plus one copy)
6. Raw data (one copy)

Microbac Laboratories, Inc., Gascoyne Division



June A. Main  
Quality Assurance Officer

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CASE NARRATIVE  
Microbac Laboratories, Inc., Gascoyne Division

Report Number: 0306390

July 8, 2003

Report To: U.S. Army Center for Health Promotion and  
Preventive Medicine (USACHPPM)  
Aberdeen Proving Ground, MD 21010-5422  
Project #DAAD05-01-D-0006      Metals

page 1 of 1

Pick-Up Order: 051/3

Date Samples Received: 06/17/03

Sample Numbers: 8455006 - 8455017, 8455022 - 8455030

Matrix: Air Filter

Twenty-one samples were transported to Microbac Laboratories, Inc., Gascoyne Division via laboratory courier and were relinquished to lab personnel in the sample control department for log-in. The sample containers were checked and were noted to be in satisfactory condition. The Field ID for sample 8455025 was incorrectly identified on the Pick-up Order, compared to the sample container. The USACHPPM COR was notified and the laboratory was instructed to correct the ID on the paperwork.

Requested test parameters performed by Microbac Laboratories, Inc., Gascoyne Division:

\* Metals analysis, using EPA SW-846 methodology

References:

Test Methods for Evaluating Solid Waste, SW-846, Third Edition, Office of Solid Waste and Emergency Response, USEPA, Wash., DC, November 1986; Final Update I, July 1992. Final Update II, September 1994. Final Update III, December 1996

(NOTE: Exceptions to the requested test parameters are as follows: The requested analysis on the Pick-up Order was EPA 200.8. Since the samples were air filters, the USACHPPM COR was notified and the laboratory was instructed to change the requested test to EPA 6020.

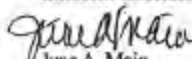
All laboratory quality control parameters were met with the following exceptions:

1. The concentrations of the Matrix Spike and Matrix Spike Duplicate (0306390-001 8455006) were inappropriate compared to the native concentration in the sample. The sample was diluted and reanalyzed. Recoveries of Post Digestion Spikes were acceptable.

Enclosed are the following:

1. Report of Analysis (original plus one copy)
2. Chain-of-Custody (original plus one copy)
3. Pick-Up Order/Delivery Order (original plus one copy)
4. Laboratory Chronicle / Case Narrative (original plus one copy)
5. Quality Control Summary Report (original plus one copy)
6. Raw data (one copy)

Microbac Laboratories, Inc., Gascoyne Division

  
June A. Main  
Quality Assurance Officer

---



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**REPORT OF ANALYSIS**

USACHPPM-Metals  
Contract #DAAD05-01-D-0006  
Bldg E2100, Rm 201  
APG, MD 21010-5422  
Attn: Richard Puzniak

Page 1

Report No. 0306390

This report of analysis contains test results for samples received at Microbac Laboratories, Inc.,  
Gascoyne Division on 6/17/2003

This Data Package contains the following:

- This Cover Page
- Sample Summary
- Test Results
- Case Narrative [Attachment]
- QC Report [Attachment]
- Terms and Conditions [Attachment]
- Chain of Custody [Attachment]

This Report of Analysis Contains 24 Pages plus Attachment(s)

Final report reviewed by:  Wen H. Pan, Ph.D. Laboratory Director

7-8-2003  
Report issue date

Microbac Laboratories, Inc. Gascoyne Division- laboratory accreditations: Maryland 109, Virginia 00152, New Jersey  
60637, Pennsylvania 68-339, New York 11158, AZLA 410.01, AJHA 100491 and US Army Corps of Engineers.



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**REPORT OF ANALYSIS**  
Sample Summary

Page 2

Client: USACHPPM-Metals  
Project: 27678-5116  
Report No: 0306390  
Date Received: 6/17/2003

Client Sample ID	Lab Sample ID	Collection Date	Collection Time
8455006 43ANAD002	0306390-001	6/3/2003	0:00
8455007 43ANAD003	0306390-002	6/3/2003	0:00
8455008 43ANAD005	0306390-003	6/3/2003	0:00
8455009 43ANAD006	0306390-004	6/3/2003	0:00
8455010 43ANAD008	0306390-005	6/3/2003	0:00
8455011 43ANAD009	0306390-006	6/3/2003	0:00
8455012 43ANAD011 (Field Blank)	0306390-007		
8455013 43ANAD012 (Trip Blank)	0306390-008		
8455014 43ANAD014	0306390-009	6/4/2003	0:00
8455015 43ANAD015	0306390-010	6/4/2003	0:00
8455016 43ANAD017	0306390-011	6/4/2003	0:00
8455017 43ANAD018	0306390-012	6/4/2003	0:00
8455022 43ANAD020	0306390-013	6/4/2003	0:00
8455023 43ANAD021	0306390-014	6/4/2003	0:00
8455024 43ANAD024	0306390-015	6/5/2003	0:00
8455025 43ANAD025	0306390-016	6/5/2003	0:00
8455026 43ANAD027	0306390-017	6/5/2003	0:00
8455027 43ANAD028	0306390-018	6/5/2003	0:00
8455028 43ANAD030	0306390-019	6/5/2003	0:00

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**REPORT OF ANALYSIS**

Page 3

**Client:** USACHPPM-Metals  
**Project:** 27678-5116  
**Report No:** 0306390  
**Date Received:** 6/17/2003

Client Sample ID	Lab Sample ID	Collection Date	Collection Time
8455029 43ANAD031	0306390-020	6/5/2003	0:00
8455030 43ANAD033 (Blank)	0306390-021		

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Test Results

Page 4

Client:	USACHPPM-Metals	Client Sample ID:	8455006 43ANAD002
Report No:	0306390	Lab ID:	0306390-001
Project:	27678-5116	Collection Date:	6/3/2003 0:00
Matrix:	FILTER		

Analytes	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				Analyst: PBK
Prep. Method: 40 CFR-50	Prep. Date: 7/1/2003 9:31:06 AM	Prep Analyst: MCA		
Chromium	24,000	150	ug/Filter	7/1/2003 19:59



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Test Results

Page 5

Client:	USACHPPM-Metals	Client Sample ID:	8455007 43ANAD003
Report No:	0306390	Lab ID:	0306390-002
Project:	27678-5116	Collection Date:	6/3/2003 0:00
Matrix:	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				
Prep. Method: 40 CFR-50	Prep. Date: 7/1/2003 9:31:08 AM	Prep Analyst: MCA	Analyst: PBK	
Chromium	12,000	60	ug/Fitter	7/1/2003 20:24


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**REPORT OF ANALYSIS**  
 Test Results

Page 6

<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455008 43ANAD005
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-003
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/3/2003 0:00
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS (EPA 6020)</b>				Analyst: PBK
Prep. Method: <u>40 CFR-50</u>	Prep. Date: <u>7/1/2003 9:31:08 AM</u>	Prep Analyst: <u>MCA</u>		
Chromium	1,800	3.0	ug/Filter	7/1/2003 15:13

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**REPORT OF ANALYSIS**  
Test Results

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Client:	USACHPPM-Metals	Client Sample ID:	8455009 43ANAD006
Report No:	0306390	Lab ID:	0306390-004
Project:	27678-5116	Collection Date:	6/3/2003 0:00
Matrix:	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS (EPA 6020)</b>				Analyst: PBK
Prep. Method: 40 CFR-50	Prep. Date: 7/1/2003 9:31:08 AM	Prep Analyst: MCA		
Chromium	810	3.0	ug/Filter	7/1/2003 15:18

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Test Results

Page 8

Client:	USACHPPM-Metals	Client Sample ID:	8455010 43ANAD008
Report No:	0306390	Lab ID:	0306390-005
Project:	27678-5116	Collection Date:	6/3/2003 0:00
Matrix:	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				Analyst: PBK
Prep. Method: 40 CFR-50	Prep. Date: 7/1/2003 9:31:05 AM	Prep Analyst: MCA		
Chromium	720	3.0	ug/Filter	7/1/2003 15:22



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**REPORT OF ANALYSIS**  
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<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455011 43ANAD009
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-006
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/3/2003 0:00
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS (EPA 6020)</b>				Analyst: PBK
Prep. Method: 40 CFR 50	Prep. Date: 7/1/2003 9:31:08 AM	Prep Analyst: MCA		
Chromium	290	3.0	ug/Filter	7/1/2003 15:27

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Client:	USACHPPM-Metals	Client Sample ID:	8455012 43ANAD011 (Field Blank)
Report No:	0306390	Lab ID:	0306390-007
Project:	27678-5116	Collection Date:	
Matrix:	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS (EPA 6020)</b>				Analyst: PBK
Prep. Method: 40 CFR-50	Prep. Date: 7/1/2003 9:31:08 AM	Prep Analyst: MCA		
Chromium	29	3.0	ug/Filter	7/1/2003 15:32




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 Test Results

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<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455013 43ANAD012 (Trip Blank)
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-008
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				
Prep. Method: 40 CFR-50	Prep. Date: 7/1/2003 9:31:08 AM		Prep Analyst: MCA	Analyst: PBK
Chromium	31	3.0	ug/Filter	7/1/2003 15:37


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 Test Results

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<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455014 43ANAD014
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-009
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/4/2003 0:00
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				<b>Analyst:</b> PBK
Prep. Method: <u>40 CFR-50</u>	Prep. Date: <u>7/1/2003 9:31:08 AM</u>	Prep Analyst: <u>MCA</u>		
Chromium	3,890	3.0	ug/Filler	7/1/2003 15:42


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 Test Results

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<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455015 43ANAD015
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-010
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/4/2003 0:00
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				Analyst: PBK
Prep. Method: <u>40 CFR-50</u>	Prep. Date: <u>7/1/2003 9:31:08 AM</u>	Prep Analyst: <u>MCA</u>		
Chromium	1,100	3.0	ug/Filter	7/1/2003 16:05

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Client:	USACHPPM-Metals	Client Sample ID:	8455016 43ANAD017
Report No:	0306390	Lab ID:	0306390-011
Project:	27678-5116	Collection Date:	6/4/2003 0:00
Matrix:	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				
Prep. Method: 40 CFR-50	Prep. Date: 7/1/2003 9:31:08 AM		Prep Analyst: MCA	Analyst: PBK
Chromium	3,600	3.0	ug/Filter	7/1/2003 16:10


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<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455017 43ANAD018
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-012
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/4/2003 0:00
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				
Prep. Method: 40 CFR-50	Prep. Date: 7/1/2003 8:31:08 AM	Prep Analyst: MCA	Analyst: PBK	
Chromium	840	3.0	ug/Filter	7/1/2003 16:15

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Test Results

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Client:	USACHPPM-Metals	Client Sample ID:	8455022 43ANAD020
Report No:	0306390	Lab ID:	0306390-013
Project:	27678-5116	Collection Date:	6/4/2003 0:00
Matrix:	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>IGPMS METALS-AIR FILTERS (EPA 6020)</b>				Analyst: PBK
Prep. Method: 40 CFR-50	Prep. Date: 7/1/2003 9:31:08 AM	Prep Analyst: MCA		
Chromium	1,600	3.0	ug/Filler	7/1/2003 16:20




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**REPORT OF ANALYSIS**  
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<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455023 43ANAD021
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-014
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/4/2003 0:00
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				
Prep. Method: 40 CFR-50	Prep. Date: 7/1/2003 9:31:08 AM	Prep Analyst: MCA	Analyst: PBK	
Chromium	710	3.0	ug/Fiter	7/1/2003 18:25


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**REPORT OF ANALYSIS**  
 Test Results

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<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455024 43ANAD024
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-013
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/5/2003 0:00
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS (EPA 6020)</b>				
Prep. Method: <u>40.CFR-50</u>	Prep. Date: <u>7/1/2003 9:31:06 AM</u>		Analyst: PBK	Prep. Analyst: MCA
Chromium	24,000	150	ug/Filter	7/1/2003 20:57


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**REPORT OF ANALYSIS**  
 Test Results

Page 19

<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455025 43ANAD025
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-016
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/5/2003 0:00
<b>Matrix:</b>	FILTER		

<b>Analyses</b>	<b>Test Results</b>	<b>Reporting Limit</b>	<b>Units</b>	<b>Date/Time Analyzed</b>
<b>ICPMS METALS-AIR FILTERS (EPA 6020)</b>				
Prep. Method: <u>40 CFR-50</u>	Prep. Date: <u>7/1/2003 9:31:08 AM</u>	Prep Analyst: <u>MCA</u>	Analyst: <u>PBK</u>	
Chromium	<b>4,900</b>	3.0	ug/Filtr	7/1/2003 16:35


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**REPORT OF ANALYSIS**  
 Test Results

Page 20

<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455026 43ANAD027
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-017
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/5/2003 0:00
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				
Prep. Method: 40 CFR-60	Prep. Date: 7/1/2003 8:31:08 AM		Prep Analyst: MCA	Analyst: PBK
Chromium	18,000	150	ug/Filter	7/1/2003 21:02


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 Test Results

Page 21

<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455027 43ANAD028
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-018
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/5/2003 0:00
<b>Matrix:</b>	FILTER		

<b>Analyses</b>	<b>Test Results</b>	<b>Reporting Limit</b>	<b>Units</b>	<b>Date/Time Analyzed</b>
<b>ICPMS METALS-AIR FILTERS (EPA 6020)</b>				
Prep. Method: 40 CFR-80	Prep. Date: 7/1/2003 9:31:08 AM		Prep Analyst: MCA	Analyst: PBK
Chromium	3,800	3.0	ug/FILTER	7/1/2003 16:45

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Client:	USACHPPM-Metals	Client Sample ID:	8455028 43ANAD030
Report No:	0306390	Lab ID:	0306390-019
Project:	27678-5116	Collection Date:	6/5/2003 0:00
Matrix:	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS (EPA 6020)</b>				Analyst: PBK
Prep. Method: 40.CFR-50	Prep. Date: 7/1/2003 9:31:08 AM	Prep Analyst: MCA		
Chromium	13,000	60	ug/Filter	7/1/2003 21:07




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**REPORT OF ANALYSIS**  
 Test Results

Page 23

<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455029 43ANAD031
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-020
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	6/5/2003 0:00
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS ( EPA 6020 )</b>				
Prep. Method: 40 CFR-90	Prep. Date: 7/1/2003 9:31:08 AM	Prep. Analyst: MCA	Analyst: PBK	
Chromium	2,000	3.0	ug/FILTER	7/1/2003 17:13


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**REPORT OF ANALYSIS**  
 Test Results

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<b>Client:</b>	USACHPPM-Metals	<b>Client Sample ID:</b>	8455030 43ANAD033 (Blank)
<b>Report No:</b>	0306390	<b>Lab ID:</b>	0306390-021
<b>Project:</b>	27678-5116	<b>Collection Date:</b>	
<b>Matrix:</b>	FILTER		

Analyses	Test Results	Reporting Limit	Units	Date/Time Analyzed
<b>ICPMS METALS-AIR FILTERS (EPA 6020)</b>				Analyst: PBK
Prep. Method: <u>40 CFR-50</u>	Prep. Date: <u>7/1/2003 9:31:08 AM</u>	Prep. Analyst: <u>MCA</u>		
Chromium	43	3.0	ug/Filter	7/1/2003 17:18

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

# APPENDIX I

## CALIBRATION PROCEDURES AND DATA

1. CALIBRATION SUMMARY. The calibration procedures are summarized in Table I-1.

Table I-1. Calibration Procedures

PARAMETER	METHOD/STANDARD	REFERENCE
Meter Box Orifice	Wet Test Meter	APTD-0576 <sup>1</sup>
Dry Gas Meter	Wet Test Meter	APTD-0576 <sup>1</sup>
Pyrometer	NBS Reference Pyrometer	USEPA RM 5 <sup>2,3</sup>
Pitot Tube	Geometry	USEPA RM 2 <sup>2,3</sup>
Thermometer/Thermocouple	Reference Pyrometer	USEPA RM 2 <sup>2,3</sup>
Nozzle	Micrometer	USEPA RM 5 <sup>2,3</sup>
Weights	Analytical Balance	USEPA RM 5 <sup>2,3</sup>
Orsat Analyzer	Calibration Gas	USEPA RM 3 <sup>2</sup>

<sup>1</sup> reference 4

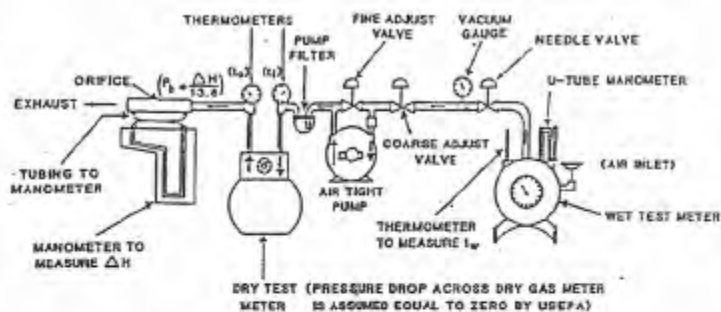
<sup>2</sup> reference 1

<sup>3</sup> reference 3

2. DRY GAS METER. The dry gas meters were calibrated prior to the assessment using a wet test meter (Figure I-1) in accordance with USEPA approved procedures. Prior to the assessment, the average dry gas meter coefficient was 1.009 for meter box 90496. The posttest calibration check was performed with the orifice setting at the average  $\Delta H$  experienced by the box during the test and the vacuum setting at the highest vacuum that occurred during the test. The posttest average dry gas meter coefficient was 1.004 for meter box 90496. All posttest calibration values were within the allowable 5-percent variation of the pretest value. The dry gas meter calibration data sheets are provided in this Appendix.

3. ORIFICE. Prior to testing, the orifice of the dry gas meter system was calibrated at the orifice manometer settings of 0.0 to 4.0 inches of water. The posttest calibration values were within the allowable 5-percent variation limit.

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$$Y = \frac{V_w P_b (t_d + 460)}{V_d \left( P_b + \frac{\Delta H}{13.6} \right) (t_w + 460)}$$

$$\Delta H @ = \frac{0.0317 (\Delta H)}{P_b (t_d + 460)} \left[ \frac{(t_w + 460) \theta}{V_w} \right]^2$$

WHERE:

$\Delta H$  = ORIFICE-PRESSURE DROP (in H<sub>2</sub>O)

$V_w$  = GAS VOLUME THROUGH WET TEST METER (ft<sup>3</sup>)

$V_d$  = GAS VOLUME THROUGH DRY GAS METER (ft<sup>3</sup>)

$t_w$  = WET TEST METER TEMP. (°F)

$t_d$  = AVERAGE DRY TEST METER TEMP. (°F)  $\left( t_d = \frac{t_1 + t_2}{2} \right)$

$P_b$  = BAROMETRIC PRESSURE (in Hg)

$\theta$  = TIME (min)

$\Delta H @$  = ORIFICE PRESSURE DROP THAT GIVES 0.75 ft<sup>3</sup>/min at 70°F, 29.92 in Hg (in H<sub>2</sub>O)

$Y$  = DIMENSIONLESS DRY GAS METER CALIBRATION COEFFICIENT

Figure I-1. Dry Gas Meter Calibration

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4. PITOT TUBE. The pitot tubes, located on the sampling probe assembly, were calibrated using the geometric standard (Figure I-2) noted in USEPA RM 2 (reference 1). Since the pitot tubes met the standard, a calibration coefficient of 0.84 was assigned to each tube. Pitot tube calibration sheets are included in this Appendix.

5. NOZZLE. As explained previously in this report, one-piece probe lines/nozzles were used in the test due to the high stack temperature. Two probe liners/nozzles were used during this assessment. The nozzle diameter for nozzle N-1 was measured with a micrometer accurate to 0.001 inch. The three measurements of the nozzle varied less than the maximum allowable tolerance of 0.004 inch. Nozzle N-1 averaged 0.249 inch diameter. These measurements were used in establishing isokinetic procedures.

6. TSP Equipment Calibration. The high-volume TSP samplers were calibrated and checked for leaks at the staging area prior to set up at the sample sites. A calibrated orifice transfer standard kit, traceable to NIST, was used to calculate each sampler's flow parameters. Calibration of the two high-volume samplers yielded acceptable correlation coefficients ( $r$ ) greater than 0.990, as required by 40 CFR Part 50, Appendix B (see Appendix A). Flow checks were performed at the beginning and end of each sampling event to ensure proper equipment operation. Periodic flow checks during sampling events were also performed. Valid samples had flow rates between 1.1 and 1.7 m<sup>3</sup>/min, and a total sample time of 2 hrs. The results of the flow checks were entered on TSP field data sheets (see Appendix G).

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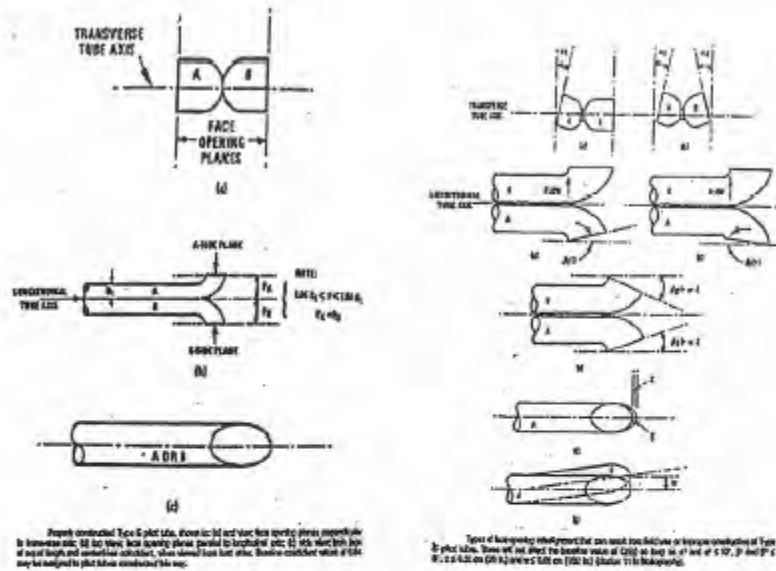


Figure I-2. Pitot Tube Geometric Calibration



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DRY GAS METER PRE/POST TEST CALIBRATION DATA SHEETS

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## METER BOX CALIBRATION DATA AND CALCULATION FORM

(English units)

Post Calibration

Date 6/12/03Meter box number 90496Barometric pressure,  $P_b = 29.92$  in. HgCalibrated by M. McCARTER

Orifice manometer setting ( $\Delta H$ ), in. H <sub>2</sub> O	Gas volume		Wet test meter ( $T_w$ ), °F	Temperatures			Time ( $t$ ), min	$Y_1$	$\Delta H$ , in. H <sub>2</sub> O
	Wet test meter ( $V_w$ ), ft <sup>3</sup>	Dry gas meter ( $V_d$ ), ft <sup>3</sup>		Dry gas meter					
				Inlet ( $T_{di}$ ), °F	Outlet ( $T_{do}$ ), °F	Avg ( $T_d$ ), °F			
1.5	5.0	5.096	71.5	92	79	85.5	7.58	1.003	1.89
1.5	5.0	5.088	71.5	92	80	86	7.57	1.006	1.88
1.5	5.0	5.097	71.5	92	80	86	7.58	1.004	1.89
Vacuum 2.5 in. Hg.								Avg 1.004	1.89

$\Delta H$ , in. H <sub>2</sub> O	$\Delta H$ 13.6	$Y_1 = \frac{V_w P_b (t_d + 460)}{V_d (P_b + \frac{\Delta H}{13.6}) (t_w + 460)}$	$\Delta H@ = \frac{0.0317 \Delta H}{P_b (t_d + 460)} \left[ \frac{(t_w + 460) \theta}{V_w} \right]$
<u>1.5</u>	<u>0.110</u>		
		Meter Box	Wet Test Meter
		Front Half Leak Check <u>OK</u>	Meter No. <u>11AL4</u>
		Back Half Leak Check <u>OK</u>	Capacity <u>1 CF/rev</u>
		Vacuum Gauge Check <u>OK</u>	Calibration Data <u>31 OCT 02</u>
		Thermometer Check (+/- 1.3° F of ASTM HG) In <u>OK</u> Out <u>OK</u>	Leak Check <u>OK</u>
			Water Level Check <u>OK</u>

\*If there is only one thermometer on the dry gas meter, record the temperature under  $t_d$ .

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PITOT TUBE CALIBRATION DATA SHEETS

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TSP SAMPLER CALIBRATION DATA SHEETS



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

## TSP SAMPLER CALIBRATION DATA SHEET

WEST

Installation:	Anniston Army Depot	Cal Date:	24 Mar 03
Site ID:	Chrome Plating Facility	Site Elev. (Ft):	N/A
Operator:	Sutphin	Sampler S/N:	0510
Pa (mm Hg):	763.0	Orifice S/N:	0113
Ta (°K):	299.0		
Equip. Type:	Graseby TSP Sampler		

Orifice Calibration Values:	m=	2.0134
Orifice Cal Date:	b=	-0.0610
	r=	0.9997

Plate Number	Delta H (in H2O)	Qstd (X) (m3/min)	Delta Pex (in H2O)	Y	Y cal.	Dev (%)
18	10.10	1.609	6.20	2.374	2.379	-0.185
13	8.10	1.444	5.00	2.132	2.137	-0.207
10	6.50	1.297	4.10	1.931	1.920	0.543
7	3.90	1.011	2.50	1.508	1.501	0.427
5	2.50	0.816	1.60	1.206	1.214	-0.660

## Standard Condition Regression

## Samplers Regression Values:

Correlation Coeff. (R)	0.9999	m=	1.4679
Intercept Coefficient (b)	0.0166	b=	0.0166
Slope (m)	1.4679	r=	0.9999
Observations	5		

## Formulas and Definitions

$$Qstd = [\Delta H (Pa/760)(298/Ta)]^{1/2} - b (1/m)$$

$$Y = [\Delta Pex (Pa/760)(298/Ta+30)]^{1/2}$$

Delta H = Cal. Orifice Pressure Drop.

Delta Pex = Sampler Motor Pressure Drop

Ycal = Sampler (m) x Qstd + Sampler (b)

Pa &amp; Ta = Ambient Bp &amp; Temp. During Cal.

Baro. pressure (Bp) elevation correction is -0.1 inch Hg per 100 feet above Sea Level.

Site Elev. = Used For Bp Correction

Qstd = X-axis

Y = Y-axis

Dev = (Y - Ycal)/Ycal(100)

Dev = + or - 5%

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### TSP SAMPLER CALIBRATION DATA SHEET

FAST

<u>Installation:</u>	Anniston Army Depot	<u>Cal Date:</u>	24 Mar 03
<u>Site ID:</u>	Chrome Plating Facility	<u>Site Elev. (Ft):</u>	N/A
<u>Operator:</u>	Sutphin	<u>Sampler S/N:</u>	6631
<u>Pa (mm Hg):</u>	763.0	<u>Orifice S/N:</u>	0113
<u>Ta (°K):</u>	299.0		
<u>Equip. Type:</u>	Graseby TSP Sampler		

<u>Orifice Calibration Values:</u>	m=	2.0134
<u>Orifice Cal Date:</u> 03/14/03	b=	-0.0610
	r=	0.9997

Plate Number	Delta H (in H <sub>2</sub> O)	Qstd (X) (m <sup>3</sup> /min)	Delta Pex (in H <sub>2</sub> O)	Y	Y cal.	Dev (%)
18	9.20	1.537	6.60	2.450	2.452	-0.097
13	7.60	1.400	5.50	2.236	2.243	-0.290
10	6.30	1.277	4.70	2.067	2.056	0.557
7	3.90	1.011	3.00	1.652	1.651	0.069
5	2.50	0.816	2.00	1.349	1.352	-0.275

Standard Condition Regression

<u>Correlation Coeff. (R)</u>	0.9999
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<u>Intercept Coefficient (b)</u>	0.1084
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<u>Slope (m)</u>	1.5247
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<u>Observations</u>	5
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Samplers Regression Values:

m=	1.5247
b=	0.1084
r=	0.9999

Formulas and Definitions

$$Qstd = [\Delta H (Pa/760)(298/Ta)]^{1/2} - b (1/m)$$

$$Y = [\Delta Pex (Pa/760)(298/Ta+30)]^{1/2}$$

Delta H= Cal. Orifice Pressure Drop.

Delta Pex= Sampler Motor Pressure Drop

Ycal = Sampler (m) x Qstd + Sampler (b)

Pa &amp; Ta= Ambient Bp &amp; Temp. During Cal.

Baro. pressure (Bp) elevation correction is -0.1 inch Hg per 100 feet above Sea Level.

Site Elev. = Used For Bp Correction

Qstd = X-axis

Y = Y-axis

Dev = (Y - Ycal)/Ycal(100)

Dev = + or - 5%

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APPENDIX J

SAMPLE CUSTODY SHEETS

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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

SAMPLE CUSTODY SHEET  
(USEPA RM 306 - TOTAL CHROMIUM)  
RUN SAMPLES

Installation: Anniston Army Depot, Alabama

Date: 4 June 2007

Project Officer: HILYARD

Project No.: 43-EL-5116-03

SAMPLE NO.	COMPONENT DESCRIPTION	VOL/ WT	RUN NO.	REMARKS
43ANAD001	Probe/FH Rinse plus Impinger Contents plus Impinger Rinse	526ml	1	0.1 N NaOH Rinse
43ANAD004	Probe/FH Rinse plus Impinger Contents plus Impinger Rinse	450ml	2	0.1 N NaOH Rinse
43ANAD007	Probe/FH Rinse plus Impinger Contents plus Impinger Rinse	450ml	3	0.1 N NaOH Rinse
43ANAD013	Probe/FH Rinse plus Impinger Contents plus Impinger Rinse	450ml	4	0.1 N NaOH Rinse
43ANAD016	Probe/FH Rinse plus Impinger Contents plus Impinger Rinse	450ml	5	0.1 N NaOH Rinse
Total Chromium				

Samples Recovered By: for M. M. CalkSamples Received By: C. D. HRelinquished By: C. D. HReceived By: for M. M. CalkRelinquished By: for M. M. CalkReceived By: Alison Dubshie

Relinquished By: \_\_\_\_\_

Received By: \_\_\_\_\_

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

SAMPLE CUSTODY SHEET  
(TSP SAMPLERS - TOTAL CHROMIUM)  
RUN SAMPLES

Installation: Anniston Army Depot, Alabama

Date: 3 June 2003

Project Officer: HILYARD

Project No.: 43-EL-5116-03

SAMPLE NO.	COMPONENT DESCRIPTION	VOL/ WT	RUN NO.	REMARKS
43ANAD 002	TSP Filter	N/A	1	Q0113427 West
43ANAD 003	TSP Filter	N/A	1	Q0113426 East
43ANAD 005	TSP Filter	N/A	2	Q0113425 West
43ANAD 006	TSP Filter	N/A	2	Q0113424 East
43ANAD 008	TSP Filter	N/A	3	Q0113423 West
43ANAD 009	TSP Filter	N/A	3	Q0113422 East
Total Chromium MET 67SF Chromium MET 701 Prep				

Samples Recovered By: [Signature]Samples Received By: [Signature]

\*\*\*\*\*

Relinquished By: [Signature]Received By: [Signature]Relinquished By: [Signature]Received By: [Signature]

Relinquished By: \_\_\_\_\_

Received By: \_\_\_\_\_



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

SAMPLE CUSTODY SHEET  
(TSP SAMPLERS - TOTAL CHROMIUM)  
RUN SAMPLES

Installation: Anniston Army Depot, Alabama

Date: 4 June 2003

Project Officer: HILYARD

Project No.: 43-EL-5116-03

SAMPLE NO.	COMPONENT DESCRIPTION	VOL./WT	RUN NO.	REMARKS
43ANAD011	TSP Filter Q0113416	N/A	Blank	Field Blank
43ANAD012	TSP Filter Q0113417	N/A	Blank	Trip Blank
43ANAD014	TSP Filter Q0113421	N/A	4	West
43ANAD015	TSP Filter Q0113420	N/A	4	East
43ANAD017	TSP Filter Q0113419	N/A	5	West
43ANAD018	TSP Filter Q0113418	N/A	5	East
Total Chromium MET676P Chromium MET701 Prep				

Samples Recovered By: [Signature]Samples Received By: [Signature]Relinquished By: [Signature]Received By: [Signature]Relinquished By: [Signature]Received By: [Signature]

Relinquished By: \_\_\_\_\_

Received By: \_\_\_\_\_

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

SAMPLE CUSTODY SHEET  
(USEPA RM 306 - TOTAL CHROMIUM)  
RUN SAMPLES

Installation: Anniston Army Depot, Alabama

Date: 4 June 2003

Project Officer: HILYARD

Project No.: 43-EL-5116-03

SAMPLE NO.	COMPONENT DESCRIPTION	VOL/ WT	RUN NO.	REMARKS
43ANAD019	Probe/FH Rinse plus Impinger Contents plus Impinger Rinse	450.6	6	0.1 N NaOH Rinse
43ANAD023	Probe/FH Rinse plus Impinger Contents plus Impinger Rinse	450.1	7	0.1 N NaOH Rinse
43ANAD026	Probe/FH Rinse plus Impinger Contents plus Impinger Rinse	450.1	8	0.1 N NaOH Rinse
43ANAD029	Probe/FH Rinse plus Impinger Contents plus Impinger Rinse	450.1	9	0.1 N NaOH Rinse
43ANAD	Probe/FH Rinse plus Impinger Contents plus Impinger Rinse			0.1 N NaOH Rinse
Total Chromium				

Samples Recovered By: for M. M. CatSamples Received By: for M. M. CatRelinquished By: for M. M. CatReceived By: for M. M. CatRelinquished By: for M. M. CatReceived By: Alphonse Bukshin

Relinquished By: \_\_\_\_\_

Received By: \_\_\_\_\_



Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

SAMPLE CUSTODY SHEET  
(TSP SAMPLERS - TOTAL CHROMIUM)  
RUN SAMPLES

Installation: Anniston Army Depot, Alabama

Date: 4 June 2003

Project Officer: HTLYARD

Project No.: 43-EL-5116-03

SAMPLE NO.	COMPONENT DESCRIPTION	VOL/ WT	RUN NO.	REMARKS
43ANAD 020	TSP Filter Q0113415	N/A	6	WEST
43ANAD 021	TSP Filter Q0113414	N/A	6	EAST
43ANAD 024	TSP Filter Q0113413	N/A	7	WEST
43ANAD 025	TSP Filter Q0113412	N/A	7	EAST
43ANAD 027	TSP Filter Q0113411	N/A	8	WEST
43ANAD 028	TSP Filter Q0113410	N/A	8	EAST
Total Chromium MET675 F Chromium MET701 Prep				

Samples Recovered By: [Signature]Samples Received By: [Signature]Relinquished By: [Signature]Received By: [Signature]Relinquished By: [Signature]Received By: [Signature]

Relinquished By: \_\_\_\_\_

Received By: \_\_\_\_\_

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

SAMPLE CUSTODY SHEET  
(TSP SAMPLERS - TOTAL CHROMIUM)  
RUN SAMPLES

Installation: Anniston Army Depot, Alabama

Date: 6 June 2003

Project Officer: HILYARD

Project No.: 43-EL-5116-03

SAMPLE NO.	COMPONENT DESCRIPTION	VOL/ WT	RUN NO.	REMARKS
43ANAD030	TSP Filter Q0113408	N/A	9	WEST
43ANAD031	TSP Filter Q0113408	N/A	9	EAST
43ANAD033	TSP Filter Q0113428	N/A	blank	Lab blank
43ANAD	TSP Filter	N/A	blank	
43ANAD	TSP Filter	N/A	blank	
43ANAD	TSP Filter	N/A		
Total Chromium MET675F Chromium MET701 Prep				

Samples Recovered By:

Samples Received By:

Relinquished By:

Received By:

Relinquished By:

Received By:

Relinquished By:

Received By:

Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

SAMPLE CUSTODY SHEET  
(USEPA RM 306 - Total Chromium)  
BLANK SAMPLES

Installation: Anniston Army Depot, Alabama , Date: 3 June 2003

Project Officer: HILYARD

Project No.: 43-EL-5116-03

SAMPLE NO.	COMPONENT DESCRIPTION	VOL/ WT	RUN NO.	REMARKS
43ANAD010	0.1 N NaOH	500 ml	- Blank	Runs 1, 2, 3
43ANAD022	0.1 N NaOH	500 ml	Blank	Runs 4-6
43ANAD032	0.1 N NaOH	500 ml	Blank	Runs 7-8
Total Chromium				

Samples Recovered By: [Signature]Samples Received By: [Signature]Relinquished By: [Signature]Received By: [Signature]Relinquished By: [Signature]Received By: [Signature]

Relinquished By: \_\_\_\_\_

Received By: \_\_\_\_\_

Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

APPENDIX K

CHROMIUM CONCENTRATION/EMISSION DATA

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Air Pollution Management Study No. 43-EL-5116-03, 3-5 June 2003

PROJECT: 43 EL-5116-03 - Zero Chromium Emission Study  
 INSTALLATION: ANNISTON ARMY DEPOT, AL  
 SOURCE: CHROME PLATING FINISHING COMPLEX, BLDG 114

Filter Dia = 0.00 in      Filter Area = 0.00 sq in  
 FH Amicro = 0.00 micrograms      BH micro = 0.00 micrograms

Blank Data:

	Cr		Mass (ug)
NaOH Blank Runs 1-3	0.6600	TSP Field Blank	29
NaOH Blank Runs 4-6	0.7600	TSP Trip Blank	31
NaOH Blank Runs 7-9	1.1000	TSP Lab Blank	43

*non-detects reported at 0.00 to allow for highest concentration*

#### Method 306

Run #	FH/BH	MBlank	TRAIN TOTAL
1	34.20	0.66	33.54
2	20.40	0.66	19.74
3	14.50	0.66	13.84
4	25.20	0.76	24.44
5	9.20	0.76	8.44
6	17.90	0.76	17.14
7	31.70	1.10	30.60
8	30.00	1.10	28.90
9	34.20	1.10	33.10

#### TSP Sampler (West)

Run #	Mass (ug)	Field Blank	Trip Blank	Lab Blank	Total
1	24000	29.000	31.000	43.000	24000
2	1800	29.000	31.000	43.000	1800
3	720	29.000	31.000	43.000	720
4	3800	29.000	31.000	43.000	3800
5	3600	29.000	31.000	43.000	3600
6	1600	29.000	31.000	43.000	1600
7	24000	29.000	31.000	43.000	24000
8	18000	29.000	31.000	43.000	18000
9	13000	29.000	31.000	43.000	13000

#### TSP Sampler (East)

Run #	Mass (ug)	Field Blank	Trip Blank	Lab Blank	Total
1	12000	29.000	31.000	43.000	12000
2	810	29.000	31.000	43.000	810
3	290	29.000	31.000	43.000	290
4	1100	29.000	31.000	43.000	1100
5	840	29.000	31.000	43.000	840
6	710	29.000	31.000	43.000	710
7	4900	29.000	31.000	43.000	4900
8	3800	29.000	31.000	43.000	3800
9	2000	29.000	31.000	43.000	2000

K-2

*values in italics indicate samples that were below analytical detection limit*

## Air Pollution Management Study No. 43-EL-5116-03, 3

PROJECT: 43 EL-5116-03 - Zero Chromium Emission Study  
 INSTALLATION: ANNISTON ARMY DEPOT, AL  
 SOURCE: CHROME PLATING FINISHING COMPLEX, BLDG 114

## CONCENTRATIONS / EMISSION RATES:

## Metals Data

Run 1	Qs (dscf/hr) =	877.212	Vm (dscf) =	76.39	TSP West Volume (m3) =	181.82
					TSP East Volume (m3) =	178.76
	Total Wt (mg)	E (lb/hr)	E (mg/hr)	Cm (mg/dscf)	TSP Concentration (mg/m3)	
Method 306	0.0335	8.49E-07	1.93E+02	0.016		
TSP Sampler (West)	24.00				0.125	
TSP Sampler (East)	12.00				0.067	
Run 2	Qs (dscf/hr) =	876.645	Vm (dscf) =	74.58	TSP West Volume (m3) =	186.80
					TSP East Volume (m3) =	178.72
	Total Wt (mg)	E (lb/hr)	E (mg/hr)	Cm (mg/dscf)	TSP Concentration (mg/m3)	
Method 306	0.0197	5.12E-07	1.19E+02	0.009		
TSP Sampler (West)	1.80				0.010	
TSP Sampler (East)	0.81				0.005	
Run 3	Qs (dscf/hr) =	826.609	Vm (dscf) =	73.87	TSP West Volume (m3) =	185.06
					TSP East Volume (m3) =	181.56
	Total Wt (mg)	E (lb/hr)	E (mg/hr)	Cm (mg/dscf)	TSP Concentration (mg/m3)	
Method 306	0.0138	3.41E-07	7.73E+01	0.007		
TSP Sampler (West)	0.72				0.004	
TSP Sampler (East)	0.28				0.002	
Run 4	Qs (dscf/hr) =	952.742	Vm (dscf) =	79.18	TSP West Volume (m3) =	186.51
					TSP East Volume (m3) =	182.92
	Total Wt (mg)	E (lb/hr)	E (mg/hr)	Cm (mg/dscf)	TSP Concentration (mg/m3)	
Method 306	0.0244	6.48E-07	1.47E+02	0.011		
TSP Sampler (West)	3.80				0.020	
TSP Sampler (East)	1.10				0.006	
Run 5	Qs (dscf/hr) =	916.163	Vm (dscf) =	70.80	TSP West Volume (m3) =	184.75
					TSP East Volume (m3) =	181.47
	Total Wt (mg)	E (lb/hr)	E (mg/hr)	Cm (mg/dscf)	TSP Concentration (mg/m3)	
Method 306	0.0084	2.22E-07	0.04E+01	0.004		
TSP Sampler (West)	3.60				0.019	
TSP Sampler (East)	0.84				0.005	
Run 6	Qs (dscf/hr) =	991.684	Vm (dscf) =	76.28	TSP West Volume (m3) =	185.72
					TSP East Volume (m3) =	179.83
	Total Wt (mg)	E (lb/hr)	E (mg/hr)	Cm (mg/dscf)	TSP Concentration (mg/m3)	
Method 306	0.0171	4.48E-07	1.02E+02	0.008		
TSP Sampler (West)	1.60				0.009	
TSP Sampler (East)	0.71				0.004	
Run 7	Qs (dscf/hr) =	952.843	Vm (dscf) =	81.07	TSP West Volume (m3) =	180.26
					TSP East Volume (m3) =	184.37
	Total Wt (mg)	E (lb/hr)	E (mg/hr)	Cm (mg/dscf)	TSP Concentration (mg/m3)	
Method 306	0.0306	7.93E-07	1.80E+02	0.013		
TSP Sampler (West)	24.00				0.130	
TSP Sampler (East)	4.80				0.027	
Run 8	Qs (dscf/hr) =	912.857	Vm (dscf) =	76.18	TSP West Volume (m3) =	184.53
					TSP East Volume (m3) =	183.98
	Total Wt (mg)	E (lb/hr)	E (mg/hr)	Cm (mg/dscf)	TSP Concentration (mg/m3)	
Method 306	0.0288	7.83E-07	1.73E+02	0.013		
TSP Sampler (West)	18.00				0.096	
TSP Sampler (East)	3.80				0.021	
Run 9	Qs (dscf/hr) =	902.542	Vm (dscf) =	76.60	TSP West Volume (m3) =	181.92
					TSP East Volume (m3) =	181.83
	Total Wt (mg)	E (lb/hr)	E (mg/hr)	Cm (mg/dscf)	TSP Concentration (mg/m3)	
Method 306	0.0331	8.61E-07	1.95E+02	0.016		
TSP Sampler (West)	15.00				0.071	
TSP Sampler (East)	2.00				0.011	

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14. ABSTRACT  This volume is an Appendix to the main report, Volume 1, which documents the demonstration of a technology developed by PRD, Inc, for control of chromium emissions during hard chromium electroplating, the Zero Emissions System. The technology involves placing a blanket of a proprietary fluid, called PRD-EL1, on top of the plating bath. This fluid blanket prevents the formation of aerosols, which is the mechanism by which chromium is emitted from the plating bath to the air. The majority of the testing was directed at demonstration of the effectiveness of chromium plating in the presence of the immiscible blanket. Testing was conducted at Benét Laboratories on coupons and actual parts from Army vehicles. The results indicate that PRD-EL1 may cause deleterious effects on the plating process, as some of the parts failed qualitative tests performed at Benét. However, some parts, which were plated without the fluid blanket present as a baseline control, also failed the tests. Air sampling results indicate that the presence of the PRD-EL1 fluid reduced the chromium emissions and indoor air concentration below standard levels. Overall, the results indicate that the use of the PRD process would require additional testing before it could be accepted for use in Army production and maintenance operations.					
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